GAS GAIN IN PROPORTIONAL COUNTERS

by

K. G. White, B.Sc.(Hons), University of Tasmania

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HOBART
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This thesis contains no material which has been submitted or accepted for the award of any other degree or diploma in any university.

To the best of my knowledge and belief, this thesis contains no material previously published or written by another person, except where due acknowledgement is made in the text.

Kenneth G. White
Kenneth G. White
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ABSTRACT

Gas gain measurements were made for nitrogen, xenon and xenon with 2,3 dimethyl-2-butene (DMB) as an additive. Two different methods of measuring gas gain were examined, pulse matching methods and current comparison methods.

A preliminary investigation was made into a new approach to the pulse matching method. Previous authors had shaped their test pulses to the same shape as their detector pulses or used a calibration factor to correct for the difference between the shape of the test pulses and the detector pulses. These approaches would be valid only if the detector pulses were always the same shape. The pulses from the detector vary in shape depending upon where the primary ion pairs are formed in the detector sensitive volume. The new approach I have investigated shapes the detector pulses and the test pulses to the same shape so that the variation in the detector pulse shape becomes irrelevant. This method of measuring gas gain was tested using P-10 and $^{148}$Gd as an alpha particle source and gave similar results to gas gains determined by current comparisons.

The measurements of gas gain finally used to obtain the data were all performed using the current comparison technique. When the electrons were collected at the central wire and $^{55}$Fe was used as the radiation source the ion saturation curves for xenon showed no definite plateaus, only points of inflexion. I found that ion saturation currents could be determined by fitting the observed currents and associated operating voltages to an expression proposed by Johnson. This expression also enabled me to determine the voltage region where gas gain began.

The gas gain characteristics of nitrogen and xenon were measured for a range of gas densities. From these measurements it was shown that the gas gain of a cylindrical proportional counter operating in the proportional region is a function only of the reduced field strength at the surface of the anode.

Aoyama has proposed an expression for the first Townsend coefficient and he has been able to show that previously proposed expressions are only special cases of his expression. I was able to obtain an excellent fit to Aoyama's expression using my gas gain data for xenon and a value for one of the parameters determined by Kowalski.

It is widely held that the mechanism of gas gain in proportional counters is primarily by electron impact. Ionization may also occur in binary mixtures by the
non-metastable Penning effect, and the metastable Penning effect. A binary mixture of xenon and DMB was used to investigate these effects. It was found that the gas gain in xenon could be greatly increased by the addition of a small quantity of DMB. A broad peak in gas gain appeared when the concentration of additive was between \( \sim 0.4\% \) and \( \sim 0.75\% \) and the molecular number density of the gas filling was \( 2.7 \times 10^{25} \text{ m}^{-3} \) (\( \sim 1 \text{ atm} \)). When the gas density was reduced to \( 1.4 \times 10^{25} \text{ m}^{-3} \) (\( \sim 0.5 \text{ atm} \)) the peak became sharper and better defined and reached its maximum when the concentration of additive was \( \sim 0.43\% \).

When the density was reduced even further to \( 7 \times 10^{24} \text{ m}^{-3} \) (\( \sim 0.26 \text{ atm} \)) the peak became even sharper and better defined centred on an additive concentration of \( \sim 0.23\% \). The gas gains used to define these peaks were of the order of \( 10^5 \), whilst in pure xenon at identical anode potentials the gas gain was of the order of 10. The mechanisms proposed for these increased gas gains were the non-metastable Penning effect and the metastable Penning effect in the case of high density mixtures, the Penning effect in the case of the intermediate density mixtures and for the low density mixtures it was suggested that doubly excited xenon molecules were ionizing the additive.

The \( W \)-values of the low density xenon plus DMB mixtures were also measured to 5\% accuracy. The trend in the mean values of these measurements indicates that the Penning effect is occurring and the minimum value in the \( W \)-value occurs at \( \sim 0.4\% \) which supports the above proposed mechanisms for the increased gas gains.

Detectors filled with mixtures of xenon plus large concentrations of DMB developed double full energy peaks in a relatively short amount of time using the \(^{55}\text{Fe} \) source. Passing a large current through the anode removed these double peaks demonstrating that the cause was uneven deposits on the anode. These deposits were probably due to polymerization of free radicals formed in the electron avalanche. Small percentages of DMB did not result in double peaks but drops in gain were observed when the detector was subjected to prolonged usage. The absence of double peaks is attributed to the diffuse nature of the avalanches. If the Penning effect or ionization of the additive by UV photons is taking place the avalanche activity would always completely surround the anode giving rise to uniform coatings around the entire circumference of the anode.
1.1 The energy resolution of a proportional counter

The total number of electrons produced in a proportional counter as a result of the formation of primary ion pairs in the counter gas and subsequent multiplication of these ion pairs by electron avalanches can be expressed by,

\[ Q = G n_0 \] (1)

where \( G \) is the gas gain, \( n_0 \) the number of primary ion pairs resulting from an energy loss \( E \), and \( Q \) the total number of electrons.

Since \( G \) and \( n_0 \) are independent of each other and the errors in \( G \) and \( n_0 \) are of a statistical nature the error propagation formula can be applied to (1).

Hence

\[ \left( \frac{\sigma_Q}{Q} \right)^2 = \left( \frac{\sigma_G}{G} \right)^2 + \left( \frac{\sigma_{n_0}}{n_0} \right)^2 \] (2)

Now \( G \) is the average gas gain of \( n_0 \) electron avalanches, i.e.

\[ G = \frac{1}{n_0} \sum_{i=1}^{n_0} A_i = \bar{A} \] (3)

where \( A_i \) is the gain in the \( i \)th electron avalanche and \( \bar{A} \) is the average gain. Applying the error propagation formula to (3) we obtain for the variance of \( G \),

\[ \sigma_G^2 = \frac{1}{n_0} \sigma_A^2 \] (4)

where \( \sigma_A^2 \) is the variance of the gas gain in a typical avalanche due to a single electron originating outside the region of gas gain.

Substituting (4) into (2) we obtain
The fluctuations in the number of primary ion pairs, \( n_0 \), for a given energy loss \( E \) may be expected to follow Poisson statistics with the variance of \( n_0 \) equal to \( n_0 \). However, Fano in 1947 [1] showed from theoretical considerations that the fluctuations should be smaller than predicted by Poisson statistics. Kirkwood et al. in 1948 [2] and Hanna et al. in 1949 [3] showed from measurements of energy resolution, that the fluctuations were smaller. The Fano-factor has been introduced to relate the observed variation with the Poisson predicted variation, i.e.

\[
\sigma_{n_0}^2 = Fn_0
\]

This gives

\[
\left( \frac{\sigma_Q}{Q} \right)^2 = \frac{1}{n_0} \left( \frac{\sigma_A}{A} \right)^2 + \frac{F}{n_0} \tag{6}
\]

Now the number of primary ion pairs, \( n_0 \), depends upon the W-value, defined as the mean energy expended to form an ion pair in the gas.

\[
n_0 = \frac{E}{W}, \text{where } E \text{ is the energy lost in the gas. Substituting into equation (6) gives}
\]

\[
\left( \frac{\sigma_Q}{Q} \right)^2 = \frac{W}{E} \left( \frac{\sigma_A}{A} \right)^2 + \frac{FW}{E} \tag{7}
\]

If the relative variance in the gas gain of an avalanche due to a single electron \((\sigma_A/A)^2\) is denoted by \( f \) equation (7) becomes

\[
\left( \frac{\sigma_Q}{Q} \right)^2 = \frac{WF}{E} + \frac{FW}{E} \tag{8}
\]
Thus if \( E/W \) is sufficiently large the values of \( Q \) will follow a gaussian distribution with standard deviation

\[
\sigma_Q = Q\sqrt{\frac{W(F + F')}{E}}
\]

The resolution \( R \) of a proportional counter is usually expressed in terms of the full width at half maximum (FWHM) of the distribution of pulse heights obtained for a given absorbed energy, \( E \), and is therefore defined as the ratio of the FWHM to the mean pulse height. The FWHM of a gaussian distribution is \( 2.35\sigma \) and therefore

\[
R = 2.35\sqrt{\frac{W(F + F')}{E}}
\]  

Equation (9) gives the parameters upon which the energy resolution of a proportional counter depend\[4,5\].

1.2 The Penning effect

The parameters \( F \) and \( W \) are constants characteristic of each particular gas or mixture of gases. In the case of xenon with electrons as the ionizing particles \( F \) is \( \leq 0.17 \) and \( W \) is 21.5 eV/ion pair [5]. It has been found that both of these parameters can be reduced under special circumstances. Some of the energy a particle loses in the counter gas goes into the formation of ion pairs and some is lost to excitation of the gas atoms or molecules. If an additive with an ionization potential lower than some of the excited states of the main gas is added to the gas the energy of these excited states might be transferred to the additive in collisions resulting in the ionization of the additive. This type of ionization is referred to as Penning ionization and the effect is called the Penning effect. There are two types of Penning effects, the metastable Penning effect (MPE) and the non-metastable Penning effect (NMPE). The MPE is the ionization of the additive by the long lived metastable states of the main counter gas and the NMPE is the ionization of the additive by the short lived non-metastable excited or resonance levels [6,7]. The Penning effect reduces the \( W \)-value and leads to a larger number of primary ion pairs for a given energy loss in the gas. This in turn will give larger pulses because each pulse will result from more electron avalanches. If the Penning effect also occurs in the electron avalanche the gas gain \( G \) will also increase. Of course to show that an increase in gas gain might be due to the Penning effect the values of both \( G \) and \( W \) should be measured for the particular gas mixture.
Sometimes a gas or vapour used as an additive to take advantage of the MPE or NMPE will have a larger W-value than the main gas, for example if 0.5% C\textsubscript{2}H\textsubscript{2} is added to Ar the W-value drops from 26.2 eV/ip (for ionization by electrons in pure Ar) to 20.3 eV/ip \cite{8}. If a large concentration of C\textsubscript{2}H\textsubscript{2} is added on the other hand the W-value of the mixture will tend towards the W-value of C\textsubscript{2}H\textsubscript{2}. In this particular case, if the additive takes part directly in the primary ionization process the W-value of the mixture will tend to increase rather than decrease. For the MPE to be effective in reducing the W-value the ionization must take place via the excited states of the Ar.

If the additive takes part directly in the ionization process the W-value of the mixture will assume some sort of "average" of the W-values of the components of the mixture. The value of this "average" will depend upon the relative concentrations of the two components. Valentine and Curran \cite{9} report that in 1950 Huber, Baldinger and Haeberli proposed an expression for the variation of the W-value of a mixture of gases as a function of the partial pressures of the component gases,

\[
\frac{1}{W_m} = \frac{S_1 P_1}{S_1 P_1 + S_2 P_2} \left( \frac{1}{W_1} + \frac{1}{W_2} \right) + \frac{1}{W_2}
\]  

where \( S_1, S_2 \) and \( P_1, P_2 \) are the stopping powers for the charged particles and partial pressures of the component gases respectively. Huber et al used \( \alpha \)-particles to obtain their experimental results and the stopping powers for these are approximately given by \( S_1 = E_\alpha/R_1 \) and \( S_2 = E_\alpha/R_2 \) where \( R_1 \) and \( R_2 \) are the ranges of the \( \alpha \)-particles in each component gas and \( E_\alpha \) is the \( \alpha \)-particle energy. Equation (10) assumes that the two gases act independently of each other. That is, a fast electron produced by the ionization of one of the atoms or molecules of one of the component gases does not ionize atoms or molecules of the other component gas. This assumption is unlikely to be valid. If we replace \( S_1 P_1/(S_1 P_1 + S_2 P_2) \) with \( Z \) (an effective atomic number) we obtain

\[
\frac{1}{W_m} = \left( \frac{1}{W_1} + \frac{1}{W_2} \right) Z + \frac{1}{W_2}
\]

That is, the reciprocal of the value of the W-value for the mixture should be linearly dependent on the effective atomic number \( Z \). Equation (11) was found to hold for only a few mixtures. Huber et al assumed that the disagreement between their results and equation (11) was due to their assumption that the delta
rays from one component gas did not ionize the other component gas. To correct for this they introduced an additional term into equation (11). Valentine et. al. [9] note that Bortner and Hurst in 1954 modified the expression for the effective atomic number to \( Z = \frac{P_1}{P_1 + aP_2} \) where the constant \( a \) has to be experimentally determined for each gas mixture. In the cases in which the previous expression for \( Z \) held \( a = S_2/S_1 \). The above expressions all ignore the Penning effect and therefore cannot be giving a correct description of the ionization processes in gas mixtures but might be useful in estimating the W-values of mixtures.

Thus, we may define a Penning mixture as a gas mixture in which ionization takes place via the excited states of the main gas. A Penning mixture, in addition to being characterized by a lower W-value also shows a lower variance in the number of primary ion pairs produced for a given energy loss. That is, a Penning mixture will have a lower Fano-factor [8]. So a Penning mixture would appear to be the ideal mixture from the point of view of energy resolution of a proportional counter.

Unfortunately, for cylindrical coaxial proportional counters, the value of \( f \), the relative variance of the gas gain in equation (9), completely dominates the resolution for gas gains greater than 10 [5].

The relative variance, \( f \) can be investigated by looking at the distributions of amplitudes of the electron avalanches due to single electrons.

**1.3 Single electron spectra**

The earliest model of an electron avalanche predicted that the distribution of avalanche sizes would follow a Furry distribution [4,10,11]. The basic assumptions of this model are: the probability of ionization by an electron during the electrons path from when it was formed until the next ionizing impact remains constant, and the energy gained from the field in one mean free path is much less than the ionization energy. With a Furry distribution the probability of a particular number of electrons being produced in an avalanche is given by,

\[
P(A) = \frac{(1 - \frac{1}{A})^{A-1}}{A}
\]  

(12)
If the average size of the avalanche is about 100 or larger as is usually the case then

\[ p(A) \equiv \left( \frac{1}{\bar{A}} \right) e^{-\frac{A}{\bar{A}}} \]  

The relative variance of this distribution is,

\[ \left( \frac{\sigma_A}{\bar{A}} \right)^2 = 1 \]  

(13)

(14)

For an average gas gain \( \bar{A} \) of 20 equation (12) predicts that 5% of all avalanches will consist of only one electron.

This situation was investigated experimentally by Curran et al in 1949 [12]. Their method enabled them to separate the variance in the number of primary ion pairs from the variance in the gas gain. This method consisted of using proportional counters with aluminium cathodes and illuminating the cathodes with UV light releasing individual photo-electrons. The cathodes were constructed in two alternative ways, by evaporating aluminium onto a quartz envelope so that the result was a semi-transparent cathode or using polished aluminium foil and inserting a quartz window to admit the UV light. The gas mixture they used consisted of a 50% Ar, 50% CH\(_4\) mixture at a pressure of 500 torr.

The efficiency of the production of electrons was about \( \sim 10^{-3} \) per quantum at UV wavelengths of 3000 to 3500 angstroms. Signals from the light source began to stand out above the noise at operating voltages of 3000 volts, and a plateau on their curve was obtained between 3700 volts and 3900 volts. Proportionality was established by comparing the pulse height spectra obtained at four different operating voltages 3145, 3280, 3550, and 3685 volts. These spectra could all be fitted closely with each other; if proportionality was being lost the pulse height distributions would have diverged from each other. The gas gain at 3550 volts was determined by other means to be 1.46x10\(^5\).

Curran et al found that the distribution of amplitudes corresponded closely with the curve \( x^{1/2} \exp(-x) \) with mean values,

\[ \bar{x} = \frac{3}{2} \]
Therefore the relative variance \( \sigma^2_x \) is 0.666 compared with the relative variance of the experimentally determined distribution of amplitudes (for \( A = 1.46 \times 10^5 \)) which is 0.696. This is different from the Furry distribution which has a relative variance of 1. Other authors have also found departures from the exponential shape predicted by the Furry distribution[9]. At low field strengths the Furry distribution seems to give a correct description of the distribution of pulse amplitudes but at high field strengths the distribution rises to a maximum value and then falls towards zero. The spread in the distribution of amplitudes is less than that predicted by the Furry distribution.

The first Townsend coefficient, \( \alpha \) is the number of ion pairs produced in a gas per unit path length by an electron moving under the influence of an electric field. It has been shown experimentally that the value of \( \alpha/N \) is a function only of the reduced field strength \( E/N \) where \( N \) is the molecular number density of the gas [13]. The functional form of \( \alpha(E) \) for xenon is shown in Chapter 9 (see Figure 9.1.1).

For a particular value of \( E \) the mean path for ionization is given by \( 1/\alpha \). The distance an electron must travel to gain enough energy from the field to ionize is given by \( U_i/E \) where \( U_i \) is the ionization potential of the gas and \( E \) is the electric field strength. If \( U_i/E \) is much less than \( 1/\alpha \), the energy to ionize must have been gained and lost in many collisions before ionization has taken place. This means that for field strengths where \( U_i/E \ll 1/\alpha \), the assumption that the probability of ionization is constant over the mean path for ionization is valid. This will occur in weak fields. In strong field strengths, \( U_i/E \sim 1/\alpha \) the assumption is no longer valid. The quantity \( \alpha U_i/E \) is a measure of the ionization efficiency and for values of \( \sim 1 \) the probability of an ionizing impact will depend upon how far the electron has travelled since the last ionizing impact [15].

Alkhazov [10] and Sephton et. al. [15] have noted that Legler proposed a model in which the distance the electron had travelled since the last ionization impact was considered. His model gave the probability distribution as
\[ P(A) = \left( \frac{1}{A} \right) \Phi \left( \frac{A}{\overline{A}} \right) \]  
(15)

where \( \Phi \) is a function which depends upon \( \alpha U_0/E \) where \( U_0 \) is the "model parameter" and \( \Phi \) must be evaluated numerically. The value of \( U_0 \) agrees with the value of \( U_1 \) to within 20% [15].

Byrne [16] proposed a model in which the mean ionization coefficient, \( \alpha(A,x) \) decreased as the number of electrons in the avalanche increased. The mean ionization coefficient is given by \( \alpha(A,x) = \alpha(x)(1 + \theta/A) \) where \( x \) is the distance through which the avalanche has been developing, \( A \) the number of electrons in the avalanche, and \( \theta \) is an empirically determined parameter. This model gave a Polya distribution as a description of the pulse amplitudes for avalanches due to single electrons in a strong field.

\[ P(A) = \left[ \frac{A(1 + \theta)}{\overline{A}} \right] \exp \left\{ \frac{-A(1 + \theta)}{\overline{A}} \right\} \]  
(16)

and

\[ \left( \frac{\sigma_A}{\overline{A}} \right)^2 = \frac{1}{A} + (1 + \theta)^{-1} \]  
(17)

According to Byrne [16] the experimental evidence as a whole tends to support equation (16). The parameter \( (1 + \theta)^{-1} \) in equation (16) is the fraction of electrons above a particular threshold. This threshold is between two and three times the ionization potential of the gas [16]. The assumption of this model, that the ionization coefficient decreases as the number of electrons in the avalanche increases, is difficult to reconcile with the experimental evidence [15]. From the point of view of the detector builder the model is not particularly useful since the probability distribution is not expressed in terms of the detector parameters.

Alkazov [10,17] has proposed a model which gives the relative variance of the gas gain in a uniform electric field as

\[ f = f_0 \left( 1 - \frac{1}{A} \right) \]  
(18)
Equation (18) shows that for small values of $A$, $f$ can be reduced. For large values of $A$, $f$ tends towards $f_0$.

$$f_0 = \frac{(2b - 1)^2}{4b - 2b^2 - 1}$$  \hspace{1cm} (19)

where

$$b = \exp\left(-\frac{\alpha U_i}{E}\right)$$  \hspace{1cm} (20)

The form of equation (19) is shown in figure 1.3.1.

![Figure 1.3.1](image)

**Figure 1.3.1**

The form of equation (19); $f_0$ is zero at $b = 1/2$. 
From equation (20) it can be seen that $f_0$ will have a fixed value in a uniform field but will be constantly changing in a cylindrical field. Equation (18) through to (20) are useful for the detector designer because they contain parameters which are related to the dimensions of the detector and the gas filling [17].

From Alkazov's work the following conclusions can be drawn; the smaller the gas gain the less the variance in the gas gain; the product of the radius of the anode wire and the gas density should be as small as possible; Penning mixtures will give reduced $W$-values and Fano-factors [5].

Table I presents a summary of some of the experimental and theoretical results for $W$, $F$, $f$ and the resolution for 5.9 keV x-rays. The values of $f$ are for gains of $\sim 100$ in cylindrical fields and the product of the gas density (or pressure) and the radius of the anode wire is 0.5 torr.cm

<table>
<thead>
<tr>
<th>GAS</th>
<th>W</th>
<th>$F(\text{calc})$</th>
<th>$F(\text{exp})$</th>
<th>f</th>
<th>R%</th>
</tr>
</thead>
<tbody>
<tr>
<td>Ne</td>
<td>36.2</td>
<td>0.17</td>
<td></td>
<td>0.45</td>
<td></td>
</tr>
<tr>
<td>Ar</td>
<td>26.2</td>
<td>0.17</td>
<td></td>
<td>0.50</td>
<td></td>
</tr>
<tr>
<td>Xe</td>
<td>21.5</td>
<td></td>
<td>$&lt;0.17$</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Ne + 0.5% Ar</td>
<td>25.3</td>
<td>0.05</td>
<td></td>
<td>0.38</td>
<td>11.6</td>
</tr>
<tr>
<td>Ar + 0.5% C$_2$H$_2$</td>
<td>20.3</td>
<td>0.075</td>
<td>$&lt;0.09$</td>
<td>0.43</td>
<td>12.2</td>
</tr>
<tr>
<td>Ar + 10% CH$_4$</td>
<td></td>
<td></td>
<td></td>
<td>0.50</td>
<td>13.2</td>
</tr>
<tr>
<td>Ar + 0.8% CH$_4$</td>
<td>26.0</td>
<td>0.17</td>
<td>$&lt;0.19$</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Ar + 20% Xe</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>12.0</td>
</tr>
</tbody>
</table>

Table 1.1
Some experimental and theoretical results for $W$, $F$, $f$ and the measured energy resolutions (R%) at 5.9 keV. The $W$-values are electron $W$-values and $f$ is for a gas gain of $\sim 100$. The product of the anode wire and the gas pressure is 0.5 torr.cm [5].

1.4 Penning mixtures and gas scintillation proportional counters

Penning mixtures are also important for gas scintillation proportional counters. The gas proportional scintillation counter is an ionization chamber capable of measuring very low energies. The idea was originally proposed by Policarpo et al in 1972 [18]. Normally low energies are only detectable by proportional counters because they operate by multiplying the electrons in the region of gas gain. The lowest energies that can be detected without gas gain are $\sim 50$ keV with cooled electronics and $\sim 800$ keV with room temperature electronics [18]. When
the primary ion pairs are formed by the energy loss from an ionizing particle or x-ray in the absorbing medium light is produced. This light signal, referred to as the primary light, is characterized by an extremely fast rise time (of the order of nanoseconds). If an electric field is applied to the chamber the electrons will drift under the influence of the applied field from points of low electrostatic potential to points of higher potential. When the electrons reach a region of a particular field strength secondary light will be produced. This secondary light is much more intense than the primary light and is characterized by a much slower rise time (of the order of microseconds). If the chamber voltage is increased or decreased the intensity of the secondary light will also increase or decrease. The secondary light, in the case of noble gas filled detectors, is the result of the de-excitation of excited noble gas molecules [19] and can be detected by a photomultiplier tube. The variance due to the photomultiplier tube is less than the variance due to gas gain when the counter is operated in the proportional mode. As a consequence of this the gas proportional scintillation counter has an energy resolution about half that of a proportional counter. The relative variance of the secondary light pulses produced by a gas proportional scintillation counter working in the ion chamber region can be expressed as

\[
\left( \frac{\sigma_N}{N} \right)^2 = \frac{F}{N_1} + V_T^2
\]

where \( N \) is the mean value of the light amplitude, \( N_1 \) the number of primary ion pairs and \( V_T^2 \) the relative variance due to the photomultiplier tube (\( V_T \approx 1/N \)) [20]. If the secondary light can be detected by a more efficient means than a photomultiplier tube the lowering of the Fano-factor may be the foremost means of improving the resolution of this class of detectors. Several other techniques for detecting the secondary light are being investigated elsewhere i.e., photoionization chambers, vacuum photodiodes, and microchannel plates [21].

1.5 Proportional counters with uniform fields

Sipila has shown [17] that for Ne - Ar Penning mixtures with 0.1% and 1.0% Ar the relative variance of the gas gain (using equation (9)) will drop to very small values for particular reduced field strengths. For the 1.0% Ar Penning mixture the relative variance drops to ~ 0.1 and in the case of 0.1% Ar to ~0.01. This implies that the electric field strength in the region of the electron avalanche should be uniform so that the reduced field strength remains constant at the optimum value. Sipila also shows that the diffusion of metastable Ne atoms has no significant effect on this minimum. He shows this by comparing the diffusion of excited atoms with that of slow neutrons in a weakly absorbing medium [17].
Marzec and Pawlowski [22] extended the work of Sipila. They found that they could get an energy resolution of 10.5% FWHM at 5.9 keV using a mixture of Ne + 1.0% CH$_4$ and a uniform field in the region of the electron avalanche. This gas filling was at a pressure of 150 torr. This resolution is not as good as the theoretically predicted resolutions for this type of detector using Penning mixtures. The theoretically predicted resolution for Ne + 0.5% Ar at 5.9 keV is 5.0%. They attribute the difference between their experimental result and the theoretical predictions to the production of secondary electrons at the cathode due to positive ion bombardment.

Sephton, Turner and Leake [15] found that the energy resolution of the Penning mixture Ne + 0.1% Ar using a uniform electric field in the region of gas multiplication was about 13% at 5.9 keV. This energy resolution is of course very good but not as good as some of the predictions.

Detectors in which the avalanche is broken up into stages were developed to cope with the problems associated with Cherenkov ring imaging in high energy physics. With this type of imaging as a means of particle identification in high energy physics it became necessary to develop detectors that were capable of detecting single UV photons with great efficiency. Ultraviolet windows have a high frequency cut-off which necessitates a gas or vapour filling with a low ionization potential. Also large gas gains must be obtainable. The requirements are contradictory since large gas gains will result in the production of UV photons and the gas filling has to be sensitive to UV photons. The multistep proportional chamber is a method of obtaining large gas gains. In this type of proportional counter the avalanche is broken up into two stages. The ion pairs are formed in a conversion region where they drift into a preamplification region and undergo some amplification. Some of these electrons are then transferred to a multiwire proportional counter where they undergo further amplification. Gas gains of about $10^6$ are obtainable with this arrangement [23].

In x-ray astronomy, good spectral resolution and good spatial resolution are both required. A uniform field gives good energy resolution but there are problems in obtaining stable operation of the detector at the gas gains ($10^4$ to $10^5$) required for good spatial resolution. A multiwire proportional counter on the other hand gives good spatial resolution. Schwarz and Mason [24] have constructed a detector they call the Penning gas imager (PGI). This detector combines Penning mixtures, two stage avalanches and uniform fields all in one detector. They have obtained resolutions of 12% FWHM at 6 keV and gas gains of 550 using Ar + 0.5% C$_2$H$_2$. This gas gain and resolution is achieved in the first stage. The second stage can boost the overall gain to $> 10^5$ to give the necessary gains required for imaging.
Ramsay and Weisskopf [25] have constructed a multistep detector incorporating both a uniform field and a multiwire proportional counter. Spectral information is obtained from the uniform field stage and the imaging information comes from the multiwire proportional counter. Figure 1.5.1 is schematic representation of their detector.

![Diagram of multistep detector](image)

Figure 1.5.1
A multistep detector taken from Ramsay and Weisskopf [25]

These authors experimented with a range of gas mixtures. For example at a gas gain of $6 \times 10^3$ they obtained an energy resolution of 13.0% at 5.9 keV using 95% Ar + 5% isobutane at pressure of one atmosphere. They obtained an energy resolution of 7.5% at 22.2 keV using a mixture of 90% Xe + 10% trimethylamine at a pressure of 0.5 atm and a gas gain of $3.5 \times 10^3$. Using equation (9) this implies an energy resolution of 14.5% at 5.9 keV. The preamplification grid separation was 4 mm and the field required to obtain a gain of $10^3$ was 7.3 kV cm$^{-1}$.

This thesis presents the results obtained from studying the effects of a particular additive on the gas gain of a xenon filled proportional counter. The two approaches to the study of gas gain are to look at the single electron spectra or to look at the amount of charge that is formed by the multiplication mechanism after a certain amount of energy has been deposited in the counter by a charged particle, x-ray, or gamma ray. In this thesis the second approach is the one used. The gas gain of each particular mixture was compared with the W-value to determine whether or not a relationship existed. The W-value measurements were absolute measurements of about 5% accuracy.
References
2.1 Introduction

There are two well known methods of measuring the gas gain of a proportional counter when the gas gain is due to the formation of $n_0$ electron avalanches where $n_0$ is the number of primary ion pairs. These methods are current comparisons (discussed in chapter 3) and pulse matching methods (discussed in chapter 6). There is another method mentioned in the literature involving measurements of pulse heights at different fill gas densities and operating voltages which will not be discussed in this thesis [1,2] The two techniques that I investigated are independent of any properties of the gas gain and are suitable for any type of proportional counter (i.e. the sealed type or the flow types).

2.2 The detectors

Two detectors were used to obtain the data presented in this thesis. Both were constructed from brass tubing of approximately the same diameter. These detectors will be referred to as detector 1 and detector 2.

Detector 1 was ~ 50 cm long with a cathode of internal diameter 3.8 cm and a 70 $\mu$m diameter tungsten anode. The detector had two beryllium windows in the cylindrical brass wall located at the centre and at one end of the detector. The detector was fitted with Kovar guard rings to prevent leakage currents flowing between the cathode and anode. Detector 1 is shown schematically in Figure 2.2.1.
Figure 2.2.1
Detector 1 is a cylindrical coaxial proportional counter with a cathode 50 cm long constructed from brass tubing. The internal diameter is 3.8 cm and the anode diameter is 70 \( \mu \text{m} \).

This counter was designed to be used with a \(^{55}\text{Fe}\) source which produces 5.9 keV \(K_\alpha\) and 6.4 keV \(K_\beta\) manganese x-rays.

Detector 2 was also constructed from brass tubing ~ 50 cm long with an internal diameter of 4.42 cm and a 70 \( \mu \text{m} \) diameter tungsten anode. This detector was fitted with ceramic insulators and had a \(^{148}\text{Gd}\) \(\alpha\)-particle source attached to the cylindrical wall. The source emits \(\alpha\)-particles of energy 3.18 MeV without emitting any \(\gamma\)-rays. The section of the wall containing the \(^{148}\text{Gd}\) source could be removed and replaced with an aluminium plug. In either case the source or plug formed part of the cylindrical wall so that minimum field distortion occurred. This detector was also fitted with guards to prevent leakage currents between the cathode and anode. Detector 2 is shown schematically in Figure 2.2.2.
Figure 2.2.2
A sectional view of detector 2. The $^{148}$Gd radiation source was attached to the inside of the brass cylindrical wall about halfway along the length of the outer electrode. The internal diameter of the brass tubing was 4.42 cm and the diameter of the tungsten wire was 70 µm. The guards were earthed because the HV was on the brass tube.

2.3 The current measurements

The electrometer used to measure the ionization currents was a Keithley model 616 digital electrometer. As an ammeter the accuracy was ±5% of the reading plus 0.1% of the range. Therefore on the $10^{-11}$ ampere range, the accuracy
would be ± 5% of the reading plus $10^{-14}$ ampere. The manufacturer's specifications give the noise as $2 \times 10^{-15}$ ampere peak to peak and the offset current as less than $5 \times 10^{-15}$ ampere.

If the count rate is extremely high the current will be steady and the electrometer can be used as an ammeter. At low count rates the current might tend to pulse so in this situation it seemed better to operate the electrometer as a coulombmeter. The current is then determined from the rate of change of charge. The errors in the current measurements made in this way are also about 5%.

As an ammeter, when measuring currents of less than $10^{-5}$ amps the input resistance of the electrometer is kept at a very low value since the range resistor is connected to the voltage amplifier in a feedback loop. ($R_{in} = \frac{R_f}{A}$ where $A$ is the open loop gain and typically about 10,000.)

When making current measurements the central wire of the detector was used as the collecting electrode and the outer electrode was attached to the high voltage supply. The following diagram is a schematic representation of the experimental set up.

![Schematic representation of the experimental arrangement for measuring currents using the electrometer as a coulombmeter. If the capacitor is replaced by a resistor the electrometer becomes an ammeter.](image-url)
2.4 Background current

The background current referred to is the current recorded when the detector is being operated in the ion chamber region (or at an operating voltage that would not result in complete charge collection) without a radiation source. This current appears to be constant and independent of the operating voltage or its polarity unless the detector is being operated in a region of gas gain. Detector 2 had an inbuilt radiation source and a background current was not measured directly. The background current recorded using detector 1 appears to be due to the establishing of a contact potential difference somewhere in the system. A constant background of $\sim +10^{-13}$ amps was recorded over a period of 14 months. The central wire was then replaced and the background was measured to be $\sim -10^{-13}$ amps independent of the operating voltage or its polarity. About 107 days later the background was observed to change from $\sim 10^{-13}$ amps to $\sim +10^{-14}$ amps during the course of an experiment. This new background seems to be permanent and identical to the background recorded prior to any changes in the central wire. The cosmic ray background and radiation from the walls of the building should produce an ionization current of $<1.2 \times 10^{-15}$ amps which would not be measurable using a Keithley 616 electrometer.
Figure 2.4.1  
An example of a background current. This background measurement was obtained using detector 1 with the outer electrode at +800 volts with respect to the inner electrode. The current is taken from the central wire which is now the cathode. The gas filling is Xe + 3.6% DMB (2,3 dimethyl - 2 - butene) at a total pressure of 200.35 torr at 0°C.

Figure 2.4.1 shows an example of how the background can change with time. If the last 100 seconds is taken to evaluate the current it becomes $+8.88 \times 10^{-14}$ amps.
Figure 2.4.2
An example of the background after the central wire had been replaced. The outer electrode was +1,000 volts with respect to the inner electrode. The current is collected from the inner electrode and the detector is filled with xenon at a pressure of 757.48 torr at 0°C. The discontinuity in the line is due to the electrometer readout changing scales.

Since the only time the background changes is when the central wire is replaced it is possible that there exists a contact potential difference between the central wire and some other surface somewhere in the system. The background current would then be the flow of charge responsible for establishing this potential difference. When the central wire was changed it was changed for a wire of the same diameter (70 µm) and the same material (tungsten). The new central wire would probably have had different surface conditions e.g. oxide layers etc. which would mean a different work function. This would mean a different contact potential difference and consequently a different current. Given time, the
changes in detector fillings and evacuations of the counter might change these surface conditions to resemble those of the old wire. The background seemed to change in a single step whereas the above reasoning implies a gradual change.

References

3.1 Current measurements using the $^{55}$Fe source

Current measurements using the $^{55}$Fe source were made with the high voltage connected to the outer electrode and the electrometer connected to the central wire. Figure 3.1.1 below shows the results obtained using operating voltages from -500 volts through to +500 volts.

![Graph showing current as a function of operating voltage.](image)

**Figure 3.1.1**
The current as a function of operating voltage from -500 volts to +500 volts using detector 1, and $^{55}$Fe. The gas filling is xenon at a pressure of 200.4 torr at 0°C.
The region in the left hand corner is a region of gas gain. Moving to the right there is no real plateau for negative voltages but a point of inflexion seems to occur at about -30 volts. The graph then turns towards zero at zero volts. For positive voltages a definite plateau seems to occur at voltages above +150 volts. This is referred to as the saturation current and is discussed more fully in chapter 4.

3.2 The measurement of gas gain

The gas gain of a cylindrical coaxial proportional counter can be determined by plotting the ionization current as a function of operating voltages. With my experimental arrangement this would mean negative operating voltages since gas gain does not occur for positive operating voltages in the range covered in my experiments [1]. If there is a region of complete charge collection prior to the onset of gas gain then curves similar to those shown in Figures 3.2.1 and 3.2.2 will be obtained. In these figures the moduli of the currents and voltages are shown. The ratio of the current at a particular operating voltage to the saturation ion current gives the gas gain at that particular operating voltage.
The ionization current as a function of operating voltage for Xe. The pressure of the gas is 206.16(26) torr at 0°C, the radiation source is $^{55}$Fe. The detector is cylindrical and coaxial with a cathode radius of 1.9 cm and an anode radius of $3.5 \times 10^{-3}$ cm (detector 1).

Figure 3.2.1

$gas \ gain = \frac{i}{i_s}$

$= 1318 \pm 93$
To minimise space charge effects when making the measurements to obtain the curves shown in Figures 3.2.1 and 3.2.2 the count rate was reduced whenever the current increased to values of $45-75 \times 10^{-11}$ A. Since there is no distinct plateau (see Figure 3.2.2) complete charge collection is assumed to occur at the point of inflexion, that is at an absolute operating voltage of about 50 volts. It will be shown in the next chapter that there is a small error incurred in taking this value.

### 3.3 Determination of W-values

If the count rate and energy deposited per count is known then the W-value (mean energy expended to produce an ion pair) can be determined. If the W-value and count rate are both known then the gain at any operating voltage can be determined by measuring the current at that voltage.
\[ i = \frac{GnEe}{W} \]

where

- \( G \) = the gas gain
- \( n \) = the count rate
- \( E \) = energy of the radiation
- \( e \) = the electronic charge

As an example, using the data I collected to produce the curves shown in Figures 3.2.1 and 3.2.2

\[
W = \frac{1318 \times 9.58 \times 10^6 \times 1.602 \times 10^{-19}}{9.40 \times 10^{-11}}
= 21.52 \pm 1.87 \text{ eV/i.p.}
\]

The current of \( 9.4 \times 10^{-11} \) amps was measured at an operating voltage of 1,200 volts. The count rate was \( 1555.4 \pm 1.2 \) cts/sec in the full energy peak and \( 181.05 \pm 0.43 \) cts/sec in the L escape peak. This corresponds to \( 9584442.2 \) eV/sec deposited in the detector.

The W-value obtained above compares well with the W-values for electrons in Xe given by Lyons et al [2] and Myers [3] which are \( 21.5 \pm 0.4 \) eV/ip and \( 21.9 \pm 0.3 \) eV/ip respectively. This topic will be discussed in greater detail in chapter 11.

References

4.1 Introduction

This chapter discusses the various factors that can effect the ionization current such as space charge effects, polarity effects, backdiffusion and the choice of radiation source.

4.2 The physics of the saturation curve

The saturation curve is the current - voltage characteristic from zero volts to the region of ion saturation. Ideally the saturation curve should show a rise in the absolute current for absolute operating voltages from 0 volts upwards until the region of saturation is reached. In this region further increases in operating voltages should not result in increases in current, hence the term ion saturation. If the electrons are being collected on the central wire eventually a region of gas gain will be encountered. Here the electrons will gain enough energy from the field in one mean free path to ionize other gas atoms or molecules. When positive ions are being collected at the central wire it is found that there is no region of gas gain [1]. The ion saturation current should be the same irrespective of whether the electrons or the positive ions are being collected on the central wire. If there are differences then there must be other physical processes adding to or subtracting from the observed saturation currents.

An example of a saturation curve obtained using the central wire as an anode is shown in Figure 4.2.1.
Figure 4.2.1
A saturation curve obtained using detector 1 filled with xenon at a pressure of 206.16 ± 0.26 torr at 0°C. The radiation source is $^{55}$Fe and the central wire is the anode.

In obtaining this curve the xenon pressure was chosen as ~200 torr at 0°C so that the 5.9 keV x-rays would not all be absorbed close to the beryllium window. At a distance of 1 cm the x-ray beam will be attenuated by a factor of 0.35 and at the central wire the initial intensity will be reduced by a factor of 0.13. Only $1.76 \times 10^{-2}$ of the initial beam intensity will strike the opposite wall of the detector.

As can be seen in Figure 4.2.1 the saturation curves I obtained from using negative operating voltages (i.e. collecting the electrons at the central wire) had no plateaus, just points of inflexion. One option available to me was to choose these points of inflexion on the current-voltage characteristics as corresponding to the saturation currents. For positive operating voltages (i.e. collection of
electrons on the outer electrode) an ion saturation curve should be obtained with no possibility of gas gain [1]. This curve should show the same saturation current as that obtained from negative operating voltages.

Figure 4.2.2 shows a comparison between the ionization curves obtained by first using the central electrode as the anode and then as the cathode.

![Figure 4.2.2](image)

**Figure 4.2.2**

Curve A was obtained using the central electrode as the anode while curve B was obtained using the central electrode as the cathode. The measurements were obtained using $^{55}$Fe, detector 1, and xenon at a pressure of 206.16 ± 0.26 torr at 0°C.

At voltages below ~ 100 V curve B shows a much poorer charge collection efficiency than curve A. Curve B is the collection of positive ions at the central wire. Lapsley [2] attributes this phenomenon to space charge effects. At low operating voltages the slowly moving positive charges moving towards the inner electrode shield the central wire from the outer electrode. When the electrons are
moving towards the central wire they are collected so quickly that relatively no build up of charge occurs and consequently insignificant shielding effects occur. If this description is correct then reducing the magnitude of the currents or reducing the count rate from the source ought to remove these space charge effects and both curves should look the same.

![Graph](attachment:image.jpg)

Figure 4.2.3
Saturation curves using detector 1, the $^{55}$Fe source and xenon at a pressure of 200.4 torr at $0^\circ$C.

The curves shown in Figure 4.2.3 were obtained about two years after the curves shown in Figure 4.2.2. The $^{55}$Fe source has a half life of approximately 2.6 years and so had decayed by an appreciable amount. In addition to the lower count rate the source was provided with some slight collimation. The saturation current has changed from $\sim 4 \times 10^{-11}$ amps to $\sim 5 \times 10^{-12}$ amps. Both curves now rise at the same rate demonstrating that the differences in the initial rises of the curves shown in Figures 4.2.2 are indeed due to space charge effects.

For the curves shown in both Figures 4.2.2 and 4.2.3 the ion saturation currents
obtained by choosing the points of inflexion (curves A) is ~20% lower than the ion saturation currents obtained by choosing the plateau regions on the other curves (curves B). This would indicate that either the point of inflexion is a bad choice or the current is different when the polarity is changed.

There are three dominant physical processes that must be overcome before ion saturation occurs: two different recombination mechanisms and diffusion of the charge against the field. The two types of recombination are initial or columnar and general or volume.

Columnar recombination occurs mainly along the high density track of ionization created by alpha particles, heavy charged ions or electrons in high pressure gases. It is important for alpha particles in gases of pressures above one atmosphere. After the initial track structure is destroyed by thermal diffusion and ionic drift volume recombination becomes the main recombination mechanism. This is where charges of the opposite sign meet and neutralize each other generally throughout the volume. Volume recombination depends upon the count rate or the current intensity whereas initial or columnar recombination depends upon the density of ionization along a particle track. These two types of recombination can be distinguished from each other by fitting the data to the following relationships;

\[
\frac{1}{i} = \frac{1}{i_s} + \frac{\text{constant}}{V} \quad (1)
\]

\[
\frac{1}{i} = \frac{1}{i_s} + \frac{\text{constant}}{V^2} \quad (2)
\]

where \(i\) is the measured current, \(V\) is the operating voltages and \(i_s\) is the ion saturation current [3]. The first relationship should hold for columnar recombination and the second for volume recombination. Of course if there are other mechanisms in addition to these removing charge from the collected current a linear fit to \(1/i\) vs \(1/V\) or \(1/i\) vs \(1/V^2\) will not be obtained.

I do not believe either of these mechanisms is affecting the collection of charge for the curves shown in Figures 4.2.2 and 4.2.3. Columnar recombination is important for alpha particles in gases at pressures above one atmosphere and I was using x-rays at pressures of ~200 torr at 0°C. Also at this pressure the x-rays are absorbed in quite a large volume making volume recombination relatively unimportant. Increasing the gas pressure would make volume recombination important and this will be demonstrated later in this chapter.
The x-rays from the $^{55}$Fe source interact with xenon by the photoelectric effect producing photoelectrons, fluorescence photons and Auger electrons. The $^{55}$Fe source emits Mn x-rays of energy 5.88765 keV, 5.89875 keV and 6.49 keV. The weighted mean value of the energy of the x-rays produced is 5.9657 keV. Xenon has three L edges at 5.453 keV, 5.107 keV and 4.787 keV. If a 5.89875 keV x-ray interacts with the 5.453 keV L edge the result can be a 0.4458 keV photoelectron and a 4.4510 keV fluorescence photon or a $\sim$3.5 keV Auger electron. The 4.4510 keV fluorescence photon can produce a $\sim$3.5 keV photoelectron from the M shell of a xenon atom elsewhere in the detector. Therefore the electrons produced by the absorption of x-rays will range in energy from $\sim$ 0.5 keV to $\sim$ 3.5 keV, the most energetic electrons being Auger electrons. Since the L - fluorescent yield of xenon is 0.23 [4] most interactions will result in the production of Auger electrons.

The practical range of electrons in xenon can be approximated by

$$\text{range} = 0.71 \, E^{1/2}$$

where the range is in g cm$^{-2}$ and $E$ is in MeV [5]. Using this relationship the range of a 3.5 keV Auger electron will be 4.237$x10^{-5}$ g cm$^{-2}$. The density of the xenon used in obtaining the curves shown in Figures 4.1.1, 4.1.2 and 4.1.3 was $\sim$ 1.5$x10^{-3}$ g cm$^{-3}$ hence the maximum range of a 3.5 keV Auger electron will be 2.7$x10^{-2}$ cm. So all the electrons produced will travel less than 0.27 mm, after which their trajectories will be determined by the thermal agitation and the influence of any electric fields present.

If the electrons are in thermal equilibrium with the gas at temperature $T$, their mean energy is $3kT/2$ leading to a mean speed at 20 °C of $v \sim 10^7$ cm s$^{-1}$. If an electric field is applied a drift velocity will be superimposed upon this mean speed. Classically this drift velocity is given by

$$w = \frac{eE}{m} \left( \frac{\lambda}{v} \right)$$

where $v$ is the mean speed, $\lambda$ the mean free path, $E$ the electric field strength and $e$ the electronic charge [6,7]. The cross section appropriate for the calculation of $\lambda$ is the momentum transfer cross section at the appropriate energy [6]. The drift velocity for electrons in xenon over a range of reduced field strengths ( $E/N$ where $N$ is the molecular number density ) can be obtained from Peisert and Sauli [7] who give the experimental results of Christophorou.

Xenon is a "hot" gas in contrast to molecular gases or noble gases with additives which are referred to as "cool" gases. If an electron drifts under the influence of an electric field in xenon its temperature will increase. If the reduced field
strength is continually increased the electron drift velocity will not saturate. With molecular gases, or mixtures of noble gases and molecular gases the drift velocity of the electrons will saturate at modest field strengths. For example, electrons drifting in xenon hydrocarbon mixtures will have a constant drift velocity for reduced field strengths above 0.5 kV/cm.atm or 1.86\times10^{-6} \text{Td} \quad (1 \text{Td} = 10^{-17} \text{volt cm}^2) \quad \text{whereas the drift velocity of electrons in pure xenon is still increasing at 3.04 kV/cm.atm or 1.13\times10^{-5} \text{Td} \quad [7]. Xenon has negligible cross sections for ionization and excitation for energies below 15 \text{eV}. At 15 \text{eV} the total collision cross section is \sim 37\times10^{-16} \text{cm}^2 \text{, the excitation cross section is} \quad 2.14\times10^{-16} \text{cm}^2 \text{ and the ionization cross section is} \quad 0.906\times10^{-16} \text{cm}^2 \quad [8]. \text{Of course some electrons must lose energy in inelastic collisions at energies of 8.32 eV (the lowest excited state of xenon) \quad [9] but the elastic cross section remains large at much higher energies. Consequently the electron temperature will continually increase as the reduced field strength increases up to energies above 15 \text{eV}.}

Consider curve A shown in Figure 4.2.2 \quad \text{. A point of inflexion occurs at} \quad 50 \text{volts}. \text{The field strength at any point inside the sensitive volume of the detector is given by}

\[ E = \frac{V}{r \ln\left(\frac{b}{a}\right)} \]

where \(V\) is the applied voltage \(r\) is the distance from the centre of the anode, \(b\) the inner radius of the cathode, and \(a\) the radius of the anode. The gas filling is xenon at a pressure of 206.16 \pm 0.26 torr at 0°C which gives a molecular number density of 7.28\times10^{24} \text{ m}^{-3} \text{ or} \quad 7.28\times10^{18} \text{ cm}^{-3}. \text{The reduced field strength can then be given in} \quad \text{volt cm}^2 \text{ or townsend's where} \quad 1 \text{Td} = 10^{-17} \text{volt cm}^2. \text{At an operating voltage of} \quad 50 \text{volts the reduced field strength just inside the cathode will be} \quad 5.74\times10^{-2} \text{Td}. \text{The drift velocity of the electrons due to the field is} \quad 6.5\times10^{4} \text{ cm sec}^{-1} \quad [7]. \text{This drift velocity will be superimposed upon the mean speed due to the electron temperature. The energies of the electrons drifting under the influence of electric fields are usually specified as characteristic energies} \quad e_K \quad \text{where} \quad e_K = kT. \text{For a reduced field strength of} \quad 0.060 \text{Td} \quad e_K = 1.19 \text{ eV} \quad [10]. \text{This gives an electron temperature of} \quad 13800 \text{ K} \text{ and a mean speed of} \quad 7.92\times10^{7} \text{ cm sec}^{-1} \text{ i.e.} \quad 1219 \text{ times the drift velocity}! \text{Moving inwards a distance of} \quad 1 \text{ cm the reduced field strength becomes} \quad 1.21\times10^{-1} \text{Td} \text{ and the characteristic energy} \quad e_K = 2.18 \text{ eV} \quad [10] \text{ giving an electron temperature of} \quad 25300 \text{ K} \text{ and a mean speed of} \quad 1.07\times10^{8} \text{ cm sec}^{-1} \text{ i.e.} \quad 1190 \text{ times the drift velocity}. 

\text{Therefore in the region within} \quad 1 \text{ cm of the window the drift velocity of the electrons has superimposed upon it a mean speed which is} \quad \sim 1,200 \text{ times greater}
than the drift velocity. As the electrons drift closer in towards the anode, the
electron temperatures continue to rise until the excitation and ionization cross
sections have grown sufficiently large to cool the drifting electrons. The fraction
of energy lost by the drifting electrons in elastic collisions is given by

\[ f = \left( \frac{8}{3} \right) \left( \frac{m}{M} \right) \]

where \( m \) is the mass of an electron and \( M \) is the mass of a xenon atom [11]. The
value of \( f \) is \( \sim 10^{-5} \) and so the loss of energy in elastic collisions can be considered
negligible. By naively extrapolating the data of Koizumi et al [10] the field
strengths corresponding to characteristic energies of 8.32 eV, 12.13 eV and 15
eV can be estimated. This will enable a rough estimate to be made of the radii at
which these energies are attained. At a radius of \( \sim 1 \) mm the electron
characteristic energy is 8.32 eV (energy level of the lowest excited state), at \( \sim 0.55 \) mm the energy rises to 12.13 eV (ionization potential of xenon) and at
0.43 mm the energy reaches 15 eV. From then on the elastic cross section begins
to decrease, the inelastic and ionization cross sections begin to increase and
presumably electron cooling takes place. It follows from this that some
additional ionization must occur near the anode as a result of the high electron
temperatures. If a xenon atom is ionized by, for example, a 15 eV electron the
result should be two low energy electrons since the ionization potential of xenon
is 12.13 eV. One of these electrons must immediately recombine since it will be
shown that diffusion with the field is probably the main process affecting
saturation.

Gas gain, in the usual sense in which the term is understood, does not occur at
50 V since an electron can obtain only a minute amount of energy from the field
in one mean free path. The momentum transfer cross section for an electron in
xenon, with energy between 4 - 10 eV is between 20 - 30 \( \times 10^{-16} \) cm\(^2\) [8]. This
gives a mean free path of about 1.6\( \times 10^{-4} \) cm. For a mean free path that ended at
the surface of the anode such an electron would gain only a maximum of 0.354
eV.

This first centimetre is also the region where most of the absorption of the \( \sim 6 \)
keV x-rays takes place. The beam is attenuated by a factor of 0.35 at 1 cm inside
the detector. In the absence of an electric field the greatest concentration of
electrons is always near the cylindrical wall. The application of an electric field
will change this concentration. If the central wire is the anode the greatest
concentration of electrons will be in the vicinity of the central wire. A diffusion
current of electrons should flow in the direction opposite to the concentration
gradient of electrons which in this case will be away from the central wire i.e. in
the same direction as the field. Therefore, there will be a loss of electrons to the
cylindrical wall which presents a large surface area.
There should be no loss of positive charge due to back diffusion. At the surface of the central wire at an operating voltage of 50 volts the field strength is 2271.4 volts cm\(^{-1}\) and the reduced field strength is 31.2 Td! Considering the large surface area of the brass cylindrical wall and the small surface area of the central wire and the intense electric field at the surface of the wire it is unlikely that a positive ion would diffuse to the central wire (anode).

Consequently, considering curve A of Figure 4.2.2 the point of inflexion at 50 volts is unlikely to represent the saturation current. The gently sloping section of the curve from 50 volts upwards probably represents a decrease in the diffusion of the electrons with the field and the subsequent loss of charge when these electrons collide with the cathode.

Diffusion of electrons in the same direction as the field seems to be the main process affecting saturation. Morton [12] found that he could not measure the ion saturation current for pressures above 4 torr for a central electrode of 1.11 cm diameter and 10 torr for a central electrode of diameter 0.32 cm. In his experiments the central electrode was operated as the cathode and the outer electrode was 8.89 cm in diameter. The ionization chamber was filled with hydrogen and the current was provided by the action of UV light on the central electrode. He was interested in studying the ionization produced by electrons in a diverging field.

Johnson [13] using a theoretical expression derived by Rice [14] which took account of the back diffusion of electrons found that he was able to measure the saturation currents in hydrogen and air for pressures in the range 0.01 torr to 760 torr. Johnson's experiments were basically an extension of the work of Morton to higher pressures. The theoretical expression he used to account for back diffusion of electrons was

\[
V = \frac{AV}{I} - B
\]

where \(V\) is the operating voltage and \(I\) the measured current. \(A\) and \(B\) are constants, \(A\) being the saturated ion current and \(B\) a constant whose value is related to the mobility of the electrons.

Applying this theoretical expression to my data straight line fits are obtained indicating that it could be a correct description of the data. The position at which departure from the straight line occurs indicates the onset of gas gain.
Figure 4.2.4
A plot of operating voltage vs V/i using the data for curve A in Figure 4.2.2, where V is the operating voltage and i the observed current. The graph is linear with a correlation coefficient $r = 0.9998$ until the operating voltage reaches 150 volts.

For instance, in Figure 4.2.4, where the operating voltage is plotted against the quotient of the operating voltage and the observed current using the data from curve A shown in Figure 4.2.2 (see Figure 4.2.4) the resulting graph is perfectly linear until an operating voltage of 150 volts is reached. This indicates that 150 volts marks the onset of gas gain. The reduced field strength at this operating voltage is 96 Td. The ion saturation current is the slope of the linear segment and the value is $4.09 \times 10^{-11}$ amps. If the point of inflexion of curve A, which occurs at 50 V, (see Figure 4.2.2) is taken as the point of complete charge collection the ion saturation current would be $3.86 \times 10^{-11}$ amps, a difference of about 6%.
Since curve B (see Figure 4.2.2) is distorted by space charge effects the current is limited by both space charge effects and backdiffusion.

![Graph showing operating voltage vs the quotient of operating voltage and observed current]

**Figure 4.2.5**
A plot of operating voltage vs the quotient of operating voltage and observed current for the data used to obtain curve A in Figure 4.1.3.

A perfectly linear plot is also obtained (see Figure 4.2.5) when plotting the operating voltage against the quotient of the operating voltage and the observed current using the data for curve A in Figure 4.2.3. This indicates that the observed current is limited only by back diffusion. The point of inflexion for curve A in Figure 4.2.3 occurs at about 30 volts and if this is taken as the point of complete charge collection the ion saturation current would be about $4.7 \times 10^{-12}$ amps. The slope of the linear segment is $5.27 \times 10^{-12}$ amps, this is interpreted to be the ion saturation current.

Reversing the polarity (see curve B in Figure 4.2.3) gives a curve with a good flat plateau from about 100 volts onwards. At 100 volts the observed current is
5.93x10^{-12} \text{amps. Between 100 volts and 500 volts the current only increases by} 1.26x10^{-13} \text{amps or 2.12\%}. A plot of the operating voltage vs the quotient of the operating voltage and the observed current is shown below (see Figure 4.2.6). This plot shows a region of changing slope which indicates that the current may be limited by other effects in addition to backdiffusion.

![Graph](image)

**Figure 4.2.6**
A plot of operating voltage vs the quotient of operating voltage and observed current using data from curve B of Figure 4.2.3.

For both curve A and curve B of Figure 4.2.3 the source was left in the same position and so the ultimate saturation ion currents should be identical. From Figure 4.2.5 the saturation ion current from curve A of Figure 4.1.3 is 5.25x10^{-12} \text{A} while from Figure 4.2.6 the saturation ion current for curve B of Figure 4.2.3 is 6.17x10^{-12} \text{A}. This current of 6.17x10^{-12} \text{A} is obtained from the upper linear segment from Figure 4.2.6 (above the region of changing slope). Curve B from Figure 4.2.3 has as already stated, a well defined plateau, and the maximum value at 500 volts is 6.05x10^{-12} \text{A}. The agreement between the
predicted ion saturation current from Figure 4.2.6 and the plateau value is good, a difference of only 1.88%.

Associated with this detector is a definite polarity effect that cannot be accounted for by back diffusion. It will be shown that this polarity effect only exists for "pure" xenon. The ion saturation current with electrons collected at the central wire is $5.25 \times 10^{-12}$ A while the ion saturation current with positive ions collected at the central wire is $6.17 \times 10^{-12}$ A. The current when the central wire is the cathode is 17.5% greater.

If the counter is being operated with the inner tungsten electrode as the anode and the brass outer electrode as the cathode electrons will strike the tungsten and positive ions will strike the brass. If electrons are liberated from either of these surfaces additional currents may flow between anode and cathode. The work function of a clean tungsten surface in a vacuum of $10^{-9}$ or $10^{-10}$ torr is about 5 eV and depends to some extent on the crystal structure of the tungsten. This work function will be different if other atoms and molecules have been adsorbed on the surface. Since the counter is filled with xenon and had been filled with a range of other gases the work function of the tungsten anode is unknown. An electron incident on the anode can be reflected or if its energy exceeds the work function of the anode a secondary electron can be emitted. Since both reflected electrons and emitted electrons are in a high field region it is expected that all electrons will eventually be collected by the anode even if they are initially reflected or emitted from the surface as secondaries.

Positive xenon ions will neutralize themselves at the brass cathode by extracting an electron from the surface. If the sum of the kinetic and potential energy of the incident xenon positive ion exceeds twice the work function of the brass a secondary electron can be emitted. I think this situation will always be the case. The work function of a clean Cu or Zn surface in a $10^{-9}$ torr or $10^{-10}$ torr vacuum is about 4.5 - 5 eV depending upon the crystal structures of the Cu or Zn. The work function of brass will of course be different and will also have adsorbed gases in its surface. Consequently the work function is unknown. How the xenon ion neutralizes itself at the surface appears to be unknown. Von Engel [15] gives the following possible sequence of events; when the positive xenon ion is a few atomic radii from the surface it extracts an electron from the brass. The now neutral xenon atom is in a metastable state for a short period of time and then it transfers its energy of excitation to the brass wall ejecting an electron by the photoelectric effect. This means that the ejected electrons should follow the Einstein $E = h \nu - W$ law (where $E$ is the energy, $h$ Planck's constant, $\nu$ frequency and $W$ is the work function) but the ejected electrons do not appear to follow this law [15]. It appears more than likely that the Xe ions do cause
secondary emission at the brass wall. These electrons will have low energy and will be in a very low field region. The brass wall presents a large surface area and I feel that most of these electrons will return to the wall.

When the counter is operated with the central electrode as the anode any secondary currents will most likely be negligible. This will not be so if the polarity is reversed. If the positive ions neutralize themselves at the central wire the secondary electrons will be produced in a high field region and will be accelerated away from the wire (cathode). Since the positive xenon ions will always have sufficient potential energy to produce secondary emission it seems likely that an additional current will flow from the central cathode to the outer anode. Consequently it seems reasonable to expect a polarity effect.

As has already been stated a polarity effect is in fact observed. The saturation ion currents for curve A and curve B of Figure 4.2.3 are $5.25 \times 10^{-12}$ A and $6.17 \times 10^{-12}$ A, i.e. the current when the central wire is the cathode is 17.5% greater. If the above explanation of this is correct then the addition of an organic quenching agent should remove this polarity effect. If the additive has an ionization potential lower than the ionization potential of the xenon then the positive ions will transfer their charge to the additive in collisions. The molecules of the additive will then become the positive charge carriers. If the additive is a complex organic molecule with many modes of excitation and vibration it will neutralize itself at the cathode absorbing the excess energy in radiationless transitions or breaking into fragments [16].

I chose 2,3 dimethyl - 2 - butene (DMB) as an additive because it has an ionization potential of $8.30 \pm 0.02$ eV [17] which is lower than the lowest excited state of xenon which is at $8.315 \pm 0.010$ eV [9]. This means that the energy from xenon atoms in metastable states can be transferred in collisions to the additive, ionizing the additive and increasing the ionization produced by the absorption of an x-ray by the gas. The DMB may not necessarily become ionized since there are other inelastic channels. For example the C-C, C-H and C=C bonds have bond energies of only 3.6 eV, 4.3 eV and 6.4 eV respectively [18], consequently dissociation of the DMB molecules into free radicals is possible.

Figure 4.2.7 below shows the current-voltage characteristic for xenon + 0.2% DMB. This amount of additive was found to have a dramatic effect on the gas gain characteristics of xenon and will be discussed in more detail in chapter 10.
Figure 4.2.7
The current-voltage characteristic for xenon + 0.2% DMB in detector 1 using a $^{55}$Fe x-ray source. The voltages are negative and applied to the outer electrode.

As can be seen from Figure 4.2.7 the addition of 0.2% DMB gives even less of a plateau than was obtainable with "pure" xenon.

Figure 4.2.8 below shows the results obtained from plotting the operating voltage against the quotient of the operating voltage and the observed current. Since the plot does not possess an initial linear segment it appears that the ionization current may not be limited only by backdiffusion.
Figure 4.2.8
A plot of absolute operating voltage against the absolute values of the quotient of the operating voltage and the observed current. The data are the same data as presented in Figure 4.2.7.

In this situation where neither columnar recombination nor volume recombination is likely to occur and the ion current appears not to be limited only by backdiffusion there is little option but to choose the point of inflexion as the point of complete charge collection. By choosing this point and calculating the gas gain at an operating voltage of 200 volts a result of 2.27 is obtained. If the current at 200 volts using the central wire as the anode is compared with the current that results from reversing the polarity and using the central wire as the cathode another figure for the gas gain can be determined. This results in a value for the gas gain of 2.16, a difference of about 5% which is the same as the accuracy of the electrometer.

The addition of the 2,3 dimethyl - 2 - butene (DMB) to the gas will have the
effect of lowering the electron temperature. The drift velocity of the electrons should now saturate. Since the DMB has many modes of vibration and excitation it should neutralize itself at an electrode via a radiationless transition or alternatively dissociate. I measured the W-value of this particular mixture by operating the counter as a proportional counter and measuring the count rate and then reversing the polarity of the detector and measuring the current associated with that count rate. The value I arrived at was 21.7 ± 1.2 eV. This is similar to the W-value for pure xenon and, in the absence of any Penning effect would appear reasonable.

Increasing the gas pressure to 753.36 torr at 0°C and using a mixture of xenon + 0.25% DMB and 226Ra as the radiation source gives the current-voltage characteristic shown below in Figure 4.2.9. High energy γ-rays from the 226Ra source produce fluorescence x-rays from the brass outer wall of the detector ionizing the gas. A small percentage of the γ-rays also interact directly with the gas by the photoelectric effect and compton scattering. With xenon the photoelectric effect is dominant at the γ-ray energies produced by the 226Ra
Figure 4.2.9
Ion saturation curve for detector 1 filled with xenon + 0.25% DMB at a pressure of 753.36 torr at 0°C. The radiation source is $^{226}$Ra.

As can be seen in Figure 4.2.9, a distinct plateau is obtained extending from about 70 volts to 130 volts. The ion saturation current obtained from this plateau is $1.62 \times 10^{-12} \pm 7.5 \times 10^{-14}$ A. At an operating voltage of 500 volts this gives a gas gain of 2.54. The gas gain at 500 volts obtained by reversing the polarity is 2.62, a difference of only 3.1%.

In summary, the addition of DMB to xenon seems to reduce the polarity effect to a value that is so small as to be undetectable considering the 5% accuracy of the current measurement.

4.3 Factors affecting the choice of radiation source

If the $^{55}$Fe is used with detector 1 filled with xenon to a pressure of 751.5 torr at
0°C, 32% of all x-rays will be absorbed in the first 1 mm and 98% of all the x-rays will be absorbed in the first 1 cm. Most of the x-rays will be absorbed close to the beryllium window in a relatively small volume. If the source is also sufficiently intense volume recombination should occur. In addition to volume recombination back diffusion will also affect the value of the observed current.

Figure 4.3.1
The ion saturation curve for detector 1 filled with xenon + 0.25% DMB at a total pressure of 753.4 torr at 0°C. The central wire is the anode and the radiation source is $^{55}$Fe. The discontinuity at 220 volts indicates a change in the electrometer sensitivity.

Figure 4.3.1 shows an ion saturation curve obtained using the $^{55}$Fe source with a mixture of xenon + 0.25% DMB at a total pressure of 753.4 torr at 0°C. The central wire is the anode and consequently gas gain is possible. As can be seen no plateau or point of inflexion occurs. Plotting $V$ vs $V/i$ does not produce a straight line indicating that processes other than back diffusion are operative.
Figure 4.3.2
An ion saturation curve for detector 1 filled with xenon + 0.25% DMB to a total pressure of 753.4 torr at 0°C. The radiation source is $^{55}$Fe and the central wire is the cathode. Once again the discontinuity at 310 volts indicates a change in the electrometer sensitivity.

Reversing the polarity of the detector so that the central wire is the cathode and using the $^{55}$Fe source does not give an ion saturation curve with a plateau (see Figure 4.3.2 above) I feel that the lack of saturation is due to volume recombination. If this is the case then using a source that does not require the beryllium window would solve the problem. The $^{226}$Ra source which consists of $^{226}$Ra and its daughter products produces x-rays of $\sim$15.5 keV and $\sim$75 keV and a range of $\gamma$-rays from 185 keV upwards. Gamma rays as energetic as 1750 keV have been detected from the source. These high energy $\gamma$-rays penetrate the brass outer cylinder and produce fluorescence x-rays in the brass walls of the counter. These fluorescence x-rays are only slightly more energetic than the $^{55}$Fe
x-rays but they will be produced along the entire length of the detector, whereas the $^{55}$Fe x-rays had to emerge from the 3mm diameter beryllium window. The photoelectrons and Compton scattered electrons from the walls of the detector will be very energetic and the subsequent ionization of the gas filling of the detector should be uniform across the diameter of the detector. The $\gamma$-rays and x-rays from the source can also interact with the gas filling itself producing ionization by pair production, photoelectric effect and Compton scattering.

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**Figure 4.3.3**

The effect of changing the radiation source from $^{55}$Fe to $^{226}$Ra. The conditions are identical to those for Figure 4.3.1.

Figure 4.3.3 above shows the change in shape of the ion saturation curve that results from changing the radiation source from $^{55}$Fe to $^{226}$Ra. The central wire is being operated as the anode and the conditions are the same as those for Figure 4.3.1. The change is quite dramatic suggesting that volume recombination may well be the reason for the lack of saturation in Figure 4.3.1.
Figure 4.3.3 is in fact identical to Figure 4.2.9 and the comments concerning Figure 4.2.9 apply once again. There is a plateau from which an ion saturation current can be determined. From this saturation current gas gains can be determined which agree to within 3.1% with the gas gains determined by reversing the polarity. Since the accuracy of the final current measurement is 5% this is considered to be adequate agreement.

4.4 Conclusion

Space charge effects were observed, using detector 1, $^{55}$Fe and a xenon filling of $\sim 200$ torr at $0^\circ$C, when the positive ions were collected at the central wire, and the saturation ion current was $\sim 4 \times 10^{-11}$ A. Reducing the current to $\sim 5 \times 10^{-12}$ A removed these space charge effects.

With xenon as a filling polarity effects are sometimes observed. The ion saturation current will be different depending upon whether the electrons or positive ions are collected at the central wire. This is probably due to positive ion bombardment producing secondary electrons at the central wire.

If the ion saturation curve has no definite plateau and the only effect removing charge from the current is backdiffusion then the ion saturation current can be determined by fitting the data for the operating voltages, $V$ and the observed currents, $i$ to the relationship $V = (AV)/i - B$ where $A$ is the saturated ion current and $B$ a constant whose value is related to the mobility of the electrons. If the relationship holds a linear fit will be obtained except where gas gain begins, consequently this relationship can also be used to determine the onset of gas gain.

The above relationship did not give a good fit with xenon plus DMB mixtures at low density (200 torr at $0^\circ$C). I found that choosing the point of inflexion when the electrons were being collected at the central wire gave a gas gain, at an operating voltage of 200 volts, of 2.27. If I reversed the polarity at 200 volts to determine the ion saturation current I obtained a value of 2.16 for the gas gain. Consequently, with these mixtures, choosing the point of inflexion does not lead to significant errors. There seem to be no significant polarity effects with xenon plus DMB mixtures.

With xenon plus DMB mixtures at pressures of $\sim 1$ atm $^{55}$Fe does not give good ion saturation curves and it is necessary to use a more penetrating source like $^{226}$Ra.
References

5.1 Introduction

Differences in energy resolution were obtained from different fillings of xenon. Sometimes the energy resolution was as good as \( \sim 17\% \) FWHM at 5.97 keV and on other occasions it was \( \sim 50\% \) FWHM at 5.97 keV with xenon fillings of \( \sim 200 \text{ torr} \) at 0°C. The samples of xenon that gave bad energy resolution may have been very pure, the bad resolution being the result of secondary electron production by xenon atoms in metastable states [1]. The xenon that gave good energy resolution may have contained some trace impurity which quenched these metastable states.

The xenon for most of the experimental work was removed from the supply company's cylinder and stored in a cylinder attached to the gas filling manifold used for evacuating and filling the detector. This cylinder had to be refilled several times from the supply company's cylinder during the experimental work.

5.2 Observations of energy resolution

After passing a current through the anode sufficient to cause it to glow red (500 mA) while the detector was under vacuum and after considerable pumping the detector was filled with xenon to a pressure of 204 torr at 0°C. The spectrum shown in Figure 5.2.1 was obtained using the \(^{55}\text{Fe}\) source.
The count rate for the above spectrum was 565 counts per second and the energy resolution is excellent (~ 17% FWHM). The operating voltage was 1200 volts. The current voltage characteristic is shown in Figure 5.2.2. The gas gain at 1200 volts is about 1700. The point of inflexion occurs on the current voltage characteristic at about 90 volts rather than the ~ 50 volts that is usually observed.
Figure 5.2.2
The current voltage characteristic for the xenon sample that gave the spectrum shown in Figure 5.2.1.

Even at a gas gain of ~12000 (operating voltage 1300 volts) and a count rate of 17000 counts per second the energy resolution at 5.97 keV was ~18% FWHM. The W-value (mean energy expended to produce an ion pair) was measured to be 21.4 ± 1.2 eV/ip which compares well with the published value of 21.5 ± 0.4 eV/ip [2]. This W-value measurement was obtained by reversing the polarity of the electrodes to obtain the ion saturation current.

The xenon for the above results, came from a cylinder attached to the manifold and showed no polarity effects. The gas gains determined by reversing the polarity to obtain ion saturation currents were identical (to within ~6%) to those obtained by comparing the currents shown in Figure 5.2.2.
The xenon cylinder attached to the manifold was then subjected to prolonged freezing with liquid nitrogen and pumping, re-freezing and pumping to remove any non-condensables. After this process a series of experiments was performed, using the detector with mixtures of the xenon and 2,3 dimethyl-2-butene. During the course of this work the cylinder on the manifold had to be replenished with xenon from the supply company's cylinder. At the conclusion of these experiments the counter was evacuated. A current large enough to cause the anode to glow red was passed through the anode to "burn off" any deposit on the anode. The counter was then filled with xenon from the cylinder on the manifold. The differential pulse height distribution obtained using this filling was quite different.

Figure 5.2.3
The differential pulse height distribution for xenon at a pressure of 204 torr at 0°C using detector 1, and $^{55}$Fe. The operating voltage is 1000 volts and the energy resolution is 40% FWHM.

The resolution had suddenly become 40% FWHM at 5.97 keV and the detector appeared unstable at 1100 volts. The count rate was 11700 counts/sec and there was a small amount of pulse pile up (about 3.5% of the pulses).

The detector was evacuated and filled to a pressure of 200 torr at 0°C with xenon suspected of being contaminated with traces of methane and air. The count rate
was approximately the same but the energy resolution was \( \sim 20\% \) FWHM at an operating voltage of 1200 volts. The gas gain at this operating voltage was about 2,863.

The xenon cylinder on the manifold was evacuated and heated moderately to \( \sim -50^\circ \text{C} \) then refilled with xenon from the supply company's cylinder. The counter was then filled from the cylinder on the manifold to a pressure of 201 torr at 0°C. This time a differential pulse height distribution was obtainable at an operating voltage of 1200 volts but the full energy peak appeared as a double peak.

The detector was filled with xenon suspected of containing traces of methane and oxygen. Prior to filling, the cylinder was frozen and pumped in an attempt to remove any non-condensables present such as methane and air. The detector was filled to a pressure of 208 torr at 0°C. A differential pulse height distribution for \(^{55}\text{Fe}\) was obtained at an operating voltage of 1200 volts and is shown below in Figure 5.3.1. The energy resolution was 20.5\% FWHM and the gas gain was 2563.3.

\[\text{counts} \quad \text{channel number}\]

\[\text{Figure 5.3.1}\]
The differential pulse height distribution for xenon at a pressure of 208 torr at 0°C. The radiation source is \(^{55}\text{Fe}\) and the operating voltage is 1200 volts giving a gas gain of about 2563.
The count rate for the above spectrum was about 24700 counts/sec and the pulse pile up is about 5.7%. The L escape peak appears at about 1450 eV (the energy of this peak should be ~ 1720 eV [3]) and the L fluorescent yield for the detector is 0.076.

The W-value of this xenon was measured by reversing the polarity to obtain an ion saturation current. The result was \(22.2 \pm 1.2 \text{ eV/ip}\) which is consistent with published values [2].

The saturation curve for this gas is excellent with a point of inflexion at about 50 volts.

The detector was then evacuated and (about six months later) filled with xenon that gave "bad" resolution. The detector was filled to a pressure of 199 torr at 0°C. The differential pulse height distribution for the \(^{55}\text{Fe}\) source is shown below in Figure 5.3.2.

![Graph of pulse height distribution](image)

**Figure 5.3.2**

The differential pulse height distribution for xenon at a pressure of 199 torr at 0°C. The radiation source is \(^{55}\text{Fe}\) and the operating voltage is 1100 volts.

The above pulse height distribution was obtained at an operating voltage of 1100
volts. The gas gain at that operating voltage was determined by current comparisons to be 320.6. The count rate was 8190 counts/sec.

If the operating voltage is increased to 1200 volts the shape of the pulse height distribution changes slightly. The peak at the higher channel number now seems to contain more pulses so that the double peaks are approximately the same height. The pulse height distribution is shown below in Figure 5.3.3.

Figure 5.3.3
A differential pulse height distribution for xenon at a pressure of 199 torr at 0°C. The radiation source was $^{55}$Fe and the operating voltage 1200 volts.

The resolution appears to be a meaningless concept when two full energy peaks are present in the spectrum. The count rate for the above spectrum was 8317 counts/sec. The gas gain at this operating voltage (1200 volts) as determined by current comparisons was 1033.8 compared with 2563 for the sample of xenon thought to contain traces of methane and air. This means that the electron avalanches are starting approximately one mean path for ionization closer to the anode. Since the pressure was slightly lower (199 torr at 0°C compared with 208 torr at 0°C) the gas gain should have been slightly higher.

At an operating voltage of 1300 volts the twin peaks seem to merge, probably as a result of a deterioration in the energy resolution.
counts

channel number

Figure 5.3.4
The differential pulse height distribution the xenon at an operating voltage of 1300 volts. The count rate is 8265 counts/sec.

On the oscilloscope, at an operating of 1300 volts, the radiation pulses seem to be followed by secondary pulses and at 1400 volts each pulse is followed by many large secondary pulses. This suggests that the positive ions might be producing secondary electrons from the brass cathode when they neutralize themselves.

5.3 Gas gain properties of the "two types" of xenon

Figure 5.3.5 below shows the current voltage characteristic for both gas fillings on the same set of axes. Both are, of course, over the region where gas gain occurs. Curve A shows a slightly larger ionization current than curve B, which may be a result of the decay of the source (\(^{55}\text{Fe}\)) since the data for curve B was collected six months after the data for curve A. It is also unlikely that the source would have been placed in exactly the same position. The difference in pressure between the two xenon fillings would have also contributed to the difference. At 500 volts in the case of curve A and 400 volts in the case of curve B the count rate was reduced to avoid space charge effects. At 750 volts in the case of curve A and 700 volts in the case of curve B the radiation source was changed from
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$^{55}$Fe to $^{226}$Ra also to minimise space charge effects. The gamma rays from the $^{226}$Ra irradiated the detector along its entire length.

![Graph](image)

**Figure 5.3.5**

A comparison of the current voltage characteristics of xenon that gives "good" energy resolution, curve A, with xenon that gives "bad" energy resolution, curve B. Both graphs are identical up to operating voltages near 1200 volts. The pressure for curve A was 208 torr and for curve B was 199 torr both at 0°C. Both curves were drawn as if the ionization current had not been weakened to avoid space charge effects in the region of gas gain.

The curves shown in Figure 5.3.5 seem to indicate that whether or not the xenon filling gives good energy resolution or poor energy resolution with double peaks the gas gain properties are similar except at the gas gains occurring near 1200 volts. The difference in the gas gains of the two fillings at this operating voltage is a factor of ~ 2.5. Current measurements in this region were made using $^{226}$Ra so the difference should not be the result of space charge effects. At the lower operating voltages the gas gains are almost identical. For example, at an
operating voltage of 1000 volts the gas gains are 242.5 for curve A and 247.3 for curve B.

For the purpose of modelling the gas gain behaviour of xenon, data from either filling should be adequate.

5.4 Conclusion

It appears that trace amounts of contaminants might drastically alter the energy resolution obtained from fillings of pure xenon but these contaminants do not significantly alter the gas gain properties of the xenon.

References

6.1 Introduction

An alternative method of measuring gas gain is the pulse matching method. This technique consists of obtaining a differential pulse height distribution and then removing the radiation source and applying a test pulse to a small capacitor connected to the input of the charge sensitive preamplifier and in parallel with the detector. The voltage amplitude of the test pulse is adjusted until the charge sensitive preamplifier is producing pulses of the same amplitude as the amplitude of the pulses that form a particular peak in the pulse height spectrum. If the capacitance of the test capacitor is small compared with the preamplifier input capacitance, and the value of the test capacitor and the voltage amplitude of the test pulses are both known, then the amount of charge required to produce the pulses for that particular peak can be calculated. Then using the W-value for the gas filling and the value for the energy of the radiation producing the peak the gas gain can be calculated. If the gas gain can be determined by an alternative method, e.g. current comparisons, then this technique can be used to determine W-values. The technique is shown schematically in Figure 6.1.1 below.

![Schematic diagram of the pulse matching method.](image)
6.2 An outline of the history of the pulse matching method

Rose and Korff [1] used this method in 1941 to obtain gas gains. They used a proportional counter with a voltage amplifier and a discriminator. The primary ionization in the counter was produced by Po $\alpha$-particles travelling parallel to the anode. To obtain the number of primary ion pairs they integrated Bragg curves taken from the literature. This gave them the number of ions produced as a function of residual range. The depth of penetration or residual range in their case was the length of the sensitive part of the counter. The discriminator was adjusted to record the largest pulses at each operating voltage. They calibrated their voltage amplifier using a test pulse generator consisting of a potential divider connected across a battery and a key connected to the amplifier input via a capacitor. This capacitor may have been a dc blocking capacitor rather than a test capacitor. The gas gain was then determined from

$$G = \frac{CP}{en_0}$$  \hspace{1cm} (1)

where $C$ is the preamplifier input capacitance, $P$ the pulse size, $e$ the charge on an electron and $n_0$ the number of primary ion pairs.

The detector pulses would have had a rise time determined by the drift velocity of the positive ions in the gas. Furthermore the preamplifier input capacitance and the bias resistor together form a differentiator that would have differentiated the pulse. This would have reduced the amplitude of the pulse. This reduction in amplitude is called the "ballistic deficit" [2]. On the other hand their pulse generator consisted of a potential divider with a key. This would have produced a step voltage. Their amplifier may have had a different gain for the relatively slowly rising detector pulse compared with the fast rising pulse generator pulse.

Rose and Ramsey [3] in 1942 developed a radically new method of measuring gas gains. This new method is the previously described current comparison technique. They point out in their 1942 paper that the pulse matching method did not permit investigation of very low gas gains whilst the current comparison method does.

Hanna et al [4] in 1949 used the pulse matching method to measure gas gains and they seemed to have used a test capacitor to measure the amount of charge injected into the system.

Diethorn [5] in 1956 studied the gas gain of proportional counters filled with methane. He determined the gas gain from the equation

$$V = \frac{EEAG}{WC}$$  \hspace{1cm} (2)

where $V$ is the amplitude of the preamplifier output pulse, $E$ is the energy lost in
the counter gas, \( A \) is the voltage gain of the preamplifier, \( C \) the total capacitance of the detector etc., \( W \) the mean energy expended to produce an ion pair in methane (28.5 eV/\( \text{ip} \)) and \( G \) the gas gain. The capacitance, \( C \), was measured using a bridge. Diethorn used a single channel analyser and a \(^{55}\text{Fe} \text{Mn} \) x-ray source as a calibration source. The amplitude of the voltage pulse at the preamplifier input necessary to produce the same peak as the \(^{55}\text{Fe} \) source was determined and from this he was able to obtain values of \( V \).

Kiser [6] in 1959 used the pulse matching method with a pulse generator that produced pulses of the same shape as those of the detector. His paper gives no details of his pulse generator or how he knew the pulses were the same shape as the detector pulses. One method would be to vary the shape of the pulses until the pulses produced by the preamplifier were similar to those produced by the absorption of radiation by the detector/preamplifier combination. He did not use a test capacitor but determined the distributed capacitance of the detector and cables. He calculated the capacitance of the detector, \( C_c \), from

\[
C_c = 0.556L \ln \left( \frac{b}{a} \right) \quad (3)
\]

where \( L \) is the length of the detector, \( b \) the cathode radius, \( a \) the anode radius and \( C_c \) is in pF. The calculated value agreed with experimentally determined values to within the experimental errors. The capacitance of the signal cable between the detector and the preamplifier was determined by altering the length of the cable and observing the amplitude of the output pulses as a function of cable length at constant operating voltage. The cable was known to have a capacitance of 6.5 pF per foot.

The voltage amplitude of a proportional counter pulse at the output of the detector can be expressed by\[7\]

\[
V(t) = V_{\text{max}} \ln \left[ 1 + \frac{t}{t_0} \right] \quad (4)
\]

where

\[
V(t) = \text{voltage across the bias resistor after a time} \ t
\]

\[
V_{\text{max}} = n_0 e G/C
\]

where

\[
n_0 = \text{number of primary ion pairs}
\]

\[
e = \text{electronic charge}
\]

\[
G = \text{gas gain}
\]

\[
C = \text{detector, cable and stray capacitance.}
\]

and
\[ t_0 = \frac{a^2 p}{2V\mu \ln\left(\frac{b}{a}\right)} \]  

where

\[ V = \text{operating voltage} \]
\[ \mu = \text{positive ion mobility} \]
\[ p = \text{gas pressure} \]

Mathieson and Charles [8] in 1969 determined the effect of equal non-interacting, integrating and differentiating time constants on the shape of the proportional counter pulse. Such a network would attenuate a step voltage by a factor of \(1/e\) (i.e. 0.3679).

They assume that the collection time of the (+)ve ions is shorter than the intrinsic time constant of the detector (detector plus bias resistor etc) and the preamplifier does not provide any shaping. If the preamplifier is followed by an RC-CR shaping network of time constant shorter than the collection time of the detector where \(RC = CR = T\) seconds then

\[ f_{\text{max}} = \frac{A}{2 \log\left(\frac{b}{a}\right)} + \frac{\text{Blog}_{10}\left(\frac{T}{t_0}\right)}{2 \log\left(\frac{b}{a}\right)} \]

where

\[ f_{\text{max}} = \text{the calibration factor} \]
\[ A = 0.087 \]
\[ B = 0.797 \]

Consider the circuit shown in Figure 6.2.1. If a test pulse of amplitude \(V_t\) is
applied to the test capacitor of capacitance $C_t$ then a charge $Q_t$ will be injected into the detector plus stray capacitance etc.. The value of $C_t$ is chosen to be small compared to input capacitance of the amplifier so that the total capacitance is effectively $C_t$. The pulse at the output of the RC-CR network due to the injection of $Q_t$ from the pulse generator will go into a particular pulse height analyzer channel, say $P_t$. Now if $Q_t$ electronic charge is formed in the detector as a result of an energy loss $E$ in the detector sensitive volume and the detector gas gain then the resulting pulse, because of its different rise time, will go into a different channel, say $P_E$. The relationship between $P_E$ and $P_t$ will be given by

$$P_E = f_{\text{max}} \cdot e^{P_t}$$

where $e = 2.718 \ldots$.

If the mobility of the positive ions is not known $f_{\text{max}}$ cannot be calculated, and the $W$-value must be known if the gas gain is to be determined.

Gott and Charles [9] have used the above expression for $f_{\text{max}}$ to determine the high field mobilities of the positive ions in various gas mixtures and then, by comparing the mobilities they obtained with published high field mobilities for various ions in the particular gas mixtures, they have been able to identify the positive charge carriers near the anode in some proportional counter gases. Since $f_{\text{max}}$ is a function of the positive ion mobility they obtained theoretical curves using unit positive ion mobilities. They then obtained experimental points and the departure of their experimental points from their theoretical curves was a measure of the departure of the positive ion mobilities from unity. For example, they determined that in Xe $+ 5\%$ CH$_4$ that the positive charge carrier was the Xe$^+$ ion in the high field region near the anode.

Hendricks [10] in 1972 extended the work of Mathieson and Charles by considering the effect of the additional differentiators existing in the signal processing chain. Consider a detector followed by preamplifier, decoupling capacitor, a differentiator and then an integrator as shown in Figure 6.2.2.
Figure 6.2.2
Detector, preamplifier, decoupling capacitor $C_t$, with a differentiation stage followed by an integration stage.

Consider the circuit shown in Figure 6.2.2. Hendricks showed that the response of the system to a step voltage which places a charge $Q_t$ across the test capacitor
$C_1$ is

$$V(t_m) = \frac{Q_1}{C_f} \frac{\tau_1}{\tau} \left[ e^{-1} - \frac{(\tau_1 + \tau_1^2)}{\tau_1^{\tau_1 - \tau}} \right] (7)$$

where $\tau = \tau_2 = \tau_3$, and $\tau << \tau_p$, and $\tau_1$ is the decoupling time constant. Also the time $t_m$ to reach the maximum pulse amplitude is given by

$$t_m = \tau \left[ 1 - \frac{\tau_1}{\tau_1^{\tau_1 - \tau}} \right] (8)$$

If the preamplifier plus amplifier employ pole-zero cancellation [11] a step voltage at the test capacitor input will be attenuated by $1/e$ where $e = 2.718...$ as in the work of Mathieson and Charles [8].

The pulse from the proportional counter is not a step function but may be expressed as

$$q(t) = -\frac{n_0 G e}{2 \ln \left( \frac{b}{a} \right)} \ln \left( \frac{2 V \mu t}{a^2 p \ln \left( \frac{b}{a} \right)} + 1 \right) (9)$$

where

- $n_0$ = the number of primary ion pairs and is given by $E/W$
- $G$ = gas gain
- $e$ = the electronic charge
- $a$ = anode radius
- $b$ = cathode radius
- $V$ = operating voltage
- $\mu$ = the mobility of the positive ions
- $p$ = gas pressure

Equation (9) assumes that all the electrons from the primary ion pairs begin avalanches at the same time, all the positive ions are formed at the central wire, and there is no recombination. The first assumption would be valid for low energy electrons ($< 10$ keV) in heavy noble gases, and the second assumption is reasonable for gas gains greater than 10 [10].
\[ q(t) = \frac{\left(\frac{E}{W}\right) Ge \ln \left(\frac{t}{t_0} + 1\right)}{2 \ln \left(\frac{b}{a}\right)} \]  

(10)

where \[t_0 = \frac{s^2 p}{2V \mu \ln \left(\frac{b}{a}\right)}\]  

(11)

The only part of equation (10) which varies with time is the \(\ln(t/t_0 + 1)\) which means that the voltage at the output of the circuit can be expressed by

\[ V(t) = \frac{Q_{pc} f(t, \tau, \tau_1, \tau_1, t_0)}{2C \ln \left(\frac{b}{a}\right)} \]  

(12)

where \(Q_{pc} = n_0 e^G\)

The function \(f(t, \tau, \tau_1, \tau_1, t_0)\) is determined by the operation of the differential equations which describe the circuit on \(\ln(t/t_0 + 1)\) and \(Q_{pc}\). The maximum voltage output may be expressed as

\[ V(t_m) = \frac{Q_{pc} K(\tau, t_0)}{2C \ln \left(\frac{b}{a}\right)} \]  

(13)

where \(K(\tau, t_0) = f(t_m, \tau, \tau_1, \tau_1, t_0)\)

To calculate \(G\) the gas gain from all this, the pulse at the output of the circuit from the pulse generator is matched on an oscilloscope screen with the pulses from a source i.e.\(^{55}\)Fe, then equation (7) and (13) can be set equal to each other.

\[ Q_{pc} = A(\tau, t_0, \frac{b}{a}) Q_t \]  

(14)

where the calibration factor

\[ A(\tau, t_0, \frac{b}{a}) = \frac{2 \ln \left(\frac{b}{a}\right)}{K(\tau, t_0)} \frac{\tau_1}{\tau_1 - \tau} \left[ e^{-1} - \frac{\left(\tau_1 + \tau_1\right)\tau_1}{\tau_1 + \tau} \left(1 - e^{-1}\right) \right] \]  

(15)

The calibration factor \(A\) shown in equations (14) and (15) is typically in the range 3 to 5.

Now the charge at the test pulse input is given by

\[ Q_t = C_t V_t \]  

(16)

Combining (14), (15), and (16) the gas gain \(G\) is given by

\[ G = \frac{A(\tau, t_0, \frac{b}{a}) C_t V_t}{\left(\frac{E}{W}\right) e} \]  

(17)

- There are two quantities that need to be known in order to apply Hendrick's
calibration factor; the drift time \( t_0 \) of the positive ions and the W-value of the counter gas. The drift time \( t_0 \) depends upon the positive ion mobility and both W-values and positive ion mobilities can be found in the literature.

The drift time \( t_0 \) can also be determined from the oscilloscope trace of the proportional counter pulse taken from the preamplifier output. This pulse can be expressed as

\[
V(t) = \frac{-n_0 Ge}{2C_i \ln\left(\frac{b}{a}\right)} \ln\left(\frac{t}{t_0}\right)
\]

A photograph of the oscilloscope trace will give \( V(t) \), then plotting \( V(t) \) against \( \ln(t) \) should give a straight line with \( \ln(t_0) \) as an intercept.

The method of calibrating the charge-sensitive preamplifier with a test pulse was most recently used by Miyahara et al [12] to determine the gas gains of 90% Ar - 10% CH\(_4\) (P - 10) over a range of pressures from 0.1 - 1.6 MPa (1 - 16 atmospheres) and for pure CH\(_4\) over the range 0.1 - 0.5 MPa. The diameters of the cathodes and anodes were varied. Three cylindrical coaxial detectors were constructed from brass for the experiments. They were; 3 cm in diameter, 15 cm long, 5 cm in diameter, 22 cm long and a third detector with a removable cathode for testing cathode diameters from 3 cm downwards. This last detector was 14 cm long. The anodes were made from stainless steel and were 22, 30, and 50 \( \mu m \) in diameter. The gas in the detector was continually flowing.

The approach of Miyahara et al [12] was to build a test pulse generator that produced a pulse that was the same shape as the proportional counter pulse. Their test capacitance was 1.27 ± 0.05 pF which immediately introduced a 4 % error into their results. The circuit for their test pulse generator is shown in Figure 6.2.3.
Figure 6.2.3
A test pulse generator that produces a pulse of the same shape as the proportional counter pulse.

The mercury relay in their circuit was operated at the mains frequency. The opening and closing of the switch switched off and on a dc power supply which produced a train of rectangular pulses. The value of the voltage produced by the dc power supply presumably could be read to a high degree of accuracy. The pulse generated square pulses were then shaped by two different RC circuits. The resulting pulses from these two RC circuits were then added together to produce a pulse of approximately the same shape as that produced by a proportional counter.

In response to a step voltage of $V_{in}$ the 0.001 µF capacitor will charge to $(120/1120)V_{in}$ volts with a time constant of $\tau \approx 107\times0.001\times10^{-6}$ seconds and the 0.02 µF capacitor will charge to $(100/220)V_{in}$ volts with a time constant of $\tau \approx 54.5\times0.02\times10^{-6}$ seconds. These two charging curves will add together to
produce a final curve of approximately the same shape as the proportional
counter pulse, the short time constant providing a fast rising section and the long
time constant producing a slow rising section. They checked that this was the
same shape as the detector pulse by shaping the pulses with two amplifiers with
different time constants (0.5 µseconds and 3 µseconds). If the two different
time constants had the same effect on the test pulses as on the proportional
counter pulses, the pulses must be the same shape.

All the approaches so far have either involved shaping the pulse so that it is the
same shape as the detector pulse or calculating the calibration factor for the
difference in the response of the preamplifier, amplifiers etc to the detector pulses
and the pulse generator pulses.

6.3 Conclusion

Gas gain measurements can be made by the pulse matching method with
accuracy provided the difference in shape between the test pulse and the detector
pulse is taken into account. Some authors shape their test pulses to the same
shape as the detector pulses while others use a calibration factor to correct for the
differences. Calibration factors have been determined by Mathieson and Charles
[8] and Hendricks [10] and a simple circuit for shaping the test pulses to the
same shape as the detector pulses has been developed by Miyahara [12].

Both of the above approaches assume that the time spread in the formation of the
electron avalanches from the primary ion pairs is small and all the positive ions
are formed in the vicinity of the anode.

References

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7.1 Introduction

This chapter describes a different approach to the pulse matching method. Instead of shaping the pulse generator pulse so that it has the same shape as the average pulse from the detector, I have constructed a circuit which shapes both the detector pulse and the pulse generator pulse to the same shape. The basic idea is shown in Figure 7.1.1.

Figure 7.1.1
An alternative approach to the pulse matching method would be to shape both the detector and pulse generator pulses to the same shape.
After the detector pulse has fully developed, the cathode is shorted by a switch and the resulting pulse is inverted so that the region of the pulse where the switch was closed becomes the pulse, i.e. the detector pulse is transformed into a step voltage at the input to the preamplifier. The switch is also closed on the test pulse in the same fashion so that both detector and test pulses are the same shape.

With the circuit shown in Figure 7.1.1 the rise time of the detector pulse is irrelevant so that it does not matter where the primary ion pairs are formed in the detector sensitive volume. This circuit, in principle at least, can be used to measure very small gas gains since it is not necessary for all the positive ions to be formed near the anode.

The accuracy of the circuit should only depend upon the precision with which the voltage amplitude of the test pulses, capacitance of the test capacitor, the $W-$values, and the energy loss in the detector are known.

7.2 The electronic circuit

The circuit is shown in Figure 7.2.1.
Figure 7.2.1
A circuit which shapes the detector pulse and the test pulse to precisely the same shape. The capacitance units not shown are in µF's.

Because the semiconductor switch (HEF 4016B) requires a signal pulse between zero and +5 V, the counter pulse is taken from the cathode. The anode is
connected directly to the high voltage, not via a high resistance.

The cathode is connected to ground via a 100 MΩ resistor, giving the detector a long differentiation time constant of ~ 7.5 ms. Other resistances to ground e.g. the insulation in the coaxial cable connecting the amplifier and detector, will have the effect of reducing the value of the 100 MΩ. The integration time constant will be the product of the resistance of the detector gas filling and the central capacitance.

The switch (HEF 4016B) when closed shorts out the cathode after the pulse has had time to fully develop, the rest of the circuit amplifies and inverts the pulse which is then received by the multichannel pulse height analyser. The pulse height analyser only accepts the (+)ve going edge of the pulse which has a height equal to the maximum pulse amplitude. This positively going section will be a step voltage with a fast rise time. The sequence is shown schematically in Figure 7.2.2.
The pulse is inverted and the capacitive coupling causes it to take on the shape indicated by the solid line.

Figure 7.2.2
The shaping sequence the pulse undergoes during its passage through the circuit.

The positive ions and electrons must be completely collected before the cathode is shorted out. The cathode should be shorted out after a period of time equal to the time it takes for the positive ions to drift from the anode to the cathode. When all the charge is collected the pulse will have attained its maximum amplitude. In order to make sure that the pulse had developed to its maximum amplitude the period of time from the detection of the pulse until the shorting of the cathode was adjustable. This time was controlled by two monostable multivibrators (HEF 4047B's). The first monostable is turned on by the detector pulse and produces a pulse with an adjustable length. The adjustment is achieved by changing the value of the variable resistor controlling the time constant of the
monostable. The inverting output of this monostable is connected to the noninverting input of a second monostable. At the conclusion of the pulse from the first monostable the second monostable produces a brief positively going pulse which enables the switch and consequently shorts out the cathode.

The experimental technique for obtaining the maximum pulse amplitude is therefore as follows; initially the length of the pulse from the first monostable is set at some small value and a pulse height distribution is obtained. Then the length of the monostable pulse is increased and another pulse height distribution is obtained. The peak of interest in the spectrum should move to a higher channel. This procedure should be repeated until the peak of interest has moved to a channel such that further repetition of the procedure causes it to move to a lower channel. Of course the count rate should be so low that no pulse pile up occurs. A $^{148}$Gd source with a low count rate ($\sim 100$ Bq) was chosen for the data presented in this thesis for this circuit. A monostable pulse length greater than $\sim 0.4$ ms was never attempted and since this gave the same pulse height distribution as a pulse length of $\sim 0.2$ ms it was assumed that the maximum pulse amplitude had occurred within $\sim 0.2$ ms.

The capacitive coupling between some of the amplification stages was necessary so that any dc voltages present were not amplified saturating subsequent amplifying stages. The first stage was a buffer amplifier providing a large input impedance ($10^{12} \Omega$). This stage together with the 100 MΩ resistor to ground helped to create a large time constant so that the detector pulse could develop to its full amplitude without any clipping due to differentiation. After the buffer is a high pass filter with a corner frequency of $f_0 = 1/(2\pi RC) = 1591.5$ Hz. This will allow the shorted section of the pulse to pass through whilst attenuating any 50 Hz pick up that might undergo amplification and subsequently trigger the monostables. The 0.01 μF capacitor also acts as dc blocking capacitor. Another similar differentiation network with the same corner frequency can be seen later on in the circuit performing a similar function.

7.3 The test pulse generator

The test pulse generator consisted of a 9 volt battery connected to a mercury wetted relay which was opened and closed 50 times a second by the mains voltage. The battery plus mercury switch were connected across a potential divider so that the pulse amplitude could be varied. The circuit is shown in Figure 7.3.1.
Figure 7.3.1
The pulse generator. By disconnecting the circuit from the mains, closing the switches marked ON and CAL the voltages determined by the potential dividers at either output can be measured with any degree of precision.

The pulse generator provided a positively going square pulse of length approximately 10 ms, with an amplitude which could be easily adjusted and measured precisely. The output shown as "output for large pulses" in Figure 7.3.1 was used to obtain the experimental results given later in this chapter. The output resistance of the pulse generator when using this particular output depends upon the amplitude of the pulses, ranging from a maximum value of about 600 $\Omega$ down to a minimum value which will be approximately the output resistance of the 9 volt battery. The mercury wetted relay will produce a pulse of rise time $\sim 1\text{ns}$ with no bounce.

7.4 The test capacitor

The capacitance of the test capacitor should be small compared with the capacitance of the detector plus the stray capacitance. Then if the test capacitor is connected in series its capacitance becomes the capacitance of the whole system. The capacitances in the system are shown schematically in Figure 7.4.1.
The capacitances of the system. If the capacitance of the test capacitor \( C_T \) is small it becomes the capacitance of the whole system.

A 1 pF test capacitor was constructed by connecting two 2.2 pF ± 0.1 pF NPO temperature compensated capacitors in series. This arrangement introduced some stray capacitance that added to the value of the second capacitor as shown schematically in Figure 7.4.2.

The stray capacitance was estimated to be \( \sim 0.2 \text{ pF} \pm 0.1 \text{ pF} \), therefore the capacitance of the test capacitor was \( 1.15 \text{ pF} \pm 0.07 \text{ pF} \).

A rough estimate of the detector plus stray capacitance is \( \sim 75 \text{ pF} \). Therefore the
capacitance of the whole system with the test capacitor connected in series is $= 1.13$ pF.

The test pulse generator produces a square wave with a period of 20 ms. By disconnecting the pulse generator from the mains and closing the two switches marked ON and CAL (see Figure 7.3.1) the voltage set by the potential divider can be measured at the output with the Keithley 616 electrometer used as a voltmeter. When used in this way the input impedance is greater than $2 \times 10^{14}$ Ω and the accuracy is 0.2% of the reading plus 0.1% of the range.

At the test pulse input the circuit is essentially a 1.13 pF capacitor. If a known voltage, $V_T$ is placed across this input the charge injected into the system, $Q$ can be calculated from $Q = CV_T$. This charge charges up the detector capacitance and the stray capacitance. After a preset time period the switch HEF 4016B (see Figure 7.3.1) shorts the cathode in precisely the same way as if the detector had been charged up by the absorption of an α-particle. Consequently the test pulse is shaped in exactly the same way as the detector pulse.

In addition to this shorting of the cathode by the circuit the positively going square pulse from the pulse generator also has a negative edge which will appear at the input of the pulse height analyser as a positively going pulse. This second pulse always had a smaller amplitude as seen on the oscilloscope and therefore appears in a lower channel. As the amplitude of the test pulse is increased the peak formed by the pulses from the negative edge moves closer to the peak formed by the pulses from shorting the cathode.

7.5 Results from the new technique

When the pulses are too small to trigger the monostables they are seen at the output as negatively going pulses. At anode potentials of +100 volts and +200 volts the output pulses from the circuit were of amplitude ~4 millivolts with what appears to be ringing on the leading edge. As the amplitude of the detector pulses is increased by increasing the anode potential the monostables begin to trigger. Both the detector pulse, and the monostable pulse which controls the length of the detector pulse, can be seen simultaneously on a double beam oscilloscope. The oscillograms below in the figures show the oscilloscope traces for anode potentials of +200 volts, +1000 volts and +1,500 volts and some samples of traces obtained from test pulses.
Figure 7.5.1
Oscillogram for an anode potential of + 200 volts. The linear amplifier is not connected and the output is taken directly from the output of the circuit. The oscilloscope is being triggered by the negative edge of the detector pulse.
Figure 7.5.2
Two oscillograms for an anode potential of +1000 volts. The top trace shows the pulse that results from shorting the cathode. The bottom trace shows the monostable pulse.
Figure 7.5.3
An oscillogram for an anode potential of +1500 volts. As in the preceding oscillograms the top trace shows the positively going pulse at the circuit output that results from shorting out the cathode. The bottom trace shows the monostable pulse.

The next series of oscillograms show how the circuit affects the pulse generator pulse. As already mentioned the pulse generator pulses are square pulses 10 ms long. Once again the top traces show the test pulse at the circuit output. Each test pulse at the test input should result in two positive output pulses, one from the shorting of the cathode and one from the negative edge of the input square pulse. The first two oscillograms (figure 7.5.4) show only the pulse that results from shorting the cathode while the next oscillogram (figure 7.5.5) also shows the pulse that results from the negative edge.
Figure 7.5.4
Oscillograms of the test pulse at the circuit output. The top trace in each oscillogram show the effect of shorting the cathode on the test pulse. The bottom trace shows the monostable pulse.
Figure 7.5.5
Oscillogram for the test pulse at the circuit output. Two positively going pulses are visible. The first positive pulse is due to shorting the cathode whilst the second is due to the negative edge of the square pulse.

In all of the oscillograms both traces are being triggered by the negative edge at the output (i.e. positive edge at the input) of either the detector pulse or the test pulse. The signal is taken directly from the circuit, i.e. there is no linear amplifier.

The major fault with the circuit is obvious in the above oscillograms (see figures 7.5.2 to 7.5.5). The monostable sees the decaying edge of the pulse formed by shorting the cathode as another positive pulse at the input and triggers again producing a secondary pulse. This secondary pulse can also trigger the monostable again.

On the leading edge of the decaying pulse a transient can be seen (it does not show up in the oscillograms). This transient has an amplitude of ≈ 0.02 volts at the circuit output and this amplitude seems to remain constant irrespective of the amplitude of the primary pulse. The secondary pulse seems to be about 0.1 of the amplitude of the radiation pulses. These idiosyncrasies do not appear to affect the results for gas gains above about 20.

For gas gains above = 20 this circuit gave results which agreed with those
determined by the current comparison technique to within a few percent. For \( \alpha \)-particle pulses and gas gains above 20 the accuracy of the final figure for the gas gain probably depends only on the accuracy to which the capacitance of the test capacitor is known and the accuracy to which the amplitude of the pulse from the pulse generator can be measured. This is assuming the capacitance of the test capacitor is small compared with the central capacitance of the system i.e. the input capacitance of the circuit. For gas gains below 20 using \(^{148}\text{Gd} \alpha\)-particles the results did not compare very well with the results obtained by current comparisons. In spite of this the results indicate that the technique is worth consideration. The only genuine fault with the circuit was that the pulses had to be large.

The detector used for all the following measurements was detector 2 (see chapter 2) and the gas filling was always P-10 at a pressure of 758.5 torr at 0°C. The series of pulse height distributions shown below illustrate the effect of letting the pulse develop for different periods of time.
The above differential pulse height distributions show the effect of increasing the monostable pulse length from 0.2 ms to 1 ms.
Since the α-particles from $^{148}\text{Gd}$ are monoenergetic ($3.182787 \pm 0.000024 \text{ MeV}$) there should be one single peak due to the alpha's that are completely absorbed by the gas. This peak corresponds to the highest energy and most prominent peak in the spectrum. The channel for this peak remains constant from one spectrum to the next. Any variation is probably due to electronic drift. It occupies channel 408, 404 and 409 in the above three spectra (see Figure 7.5.6 above). This would indicate that a monostable pulse length of 0.2 ms is sufficient to allow the detector pulse to develop to its maximum amplitude. It also means that the pulse does not decay to any measurable extent during the next 0.8 ms. Thus the detector differentiation time constant is long enough.

The increase in pulse length seems to have the effect of developing a ridge on the low energy side of the main peak in the spectrum. The slope of the low energy side is probably the result of numerous α-particles depositing part of their energy in the wall of the counter. This distortion in the low energy side may be the result of pulse pile up among these low energy pulses. This idea is supported by the decrease in the number of counts in the main peak 56969 counts/sec decreased to 47906 counts/sec. The larger pulse length would certainly increase pulse pile up. The pulse matching technique gives a gas gain at $+1300$ volts of $21.66 \pm 1.40$ while current comparisons give $23.01\pm1.47$.

The following pulse height distributions show the effect of monostable pulse lengths of 50 µs, 0.2 ms and 0.4 ms for an operating voltage of $+1700$ volts. The data were collected over a period of two days and the spectra were not obtained in the order shown.
monostable pulse length = 50 µs
anode potential = +1700 volts
pulse height distribution obtained over 1k secs
counts between channel 595 and 352 = 52359 cts

pulse height distribution obtained over 100 secs
amplitude of test pulse = 3.26 volts
charge injected = 3.26x1.13x10^{-12} C
gas gain = 187.82±12.18

Figure 7.5.7
If the monostable pulse length is set at 50 µs and the W-value for 3.182787(24) MeV alpha particles in P-10 is taken as 26.0 eV/ip ± 0.5 eV/ip the gas gain given by the pulse matching method is 187.82±12.18. Current comparisons give a value of 228.77 ± 14.64.
Figure 7.5.8
The monostable pulse length is increased to 0.2 ms. The gas gain given by the pulse matching method is 210.29 ± 13.64. Current comparisons give a value of 228.77 ± 14.64.
The monostable pulse length increased to 0.4 ms. A distortion now appears on the low energy side but the position of the peak does not change.

The test pulse spectrum illustrated in figures 7.5.7 and 7.5.8 show two peaks. As already mentioned the peak in the lower energy channel corresponds to the negative edge of the input square wave and the other corresponds to the shorting of the cathode by the circuit. These test pulse peaks are only a few channels wide.

As the monostable pulse width is increased from 50 µs to 0.2 ms the position of the peak changes from channel ≈ 510 to ≈ 550. This is a significant change. The gas gain as calculated by the pulse matching method changes from 187.82 to 210.29. The errors in the values are due to the uncertainties in the test capacitor and the W value which of course remain constant. This test capacitor is NPO temperature compensated. The errors in the gas gains can therefore be ignored and the two figures can be compared directly. Increasing the monostable pulse length from 50 µs to 0.2 ms results in a 11.96% increase in the value for the gas gain.

Increasing the monostable pulse length from 0.2 ms to 0.4 ms makes no difference to the position of the main peak (see Figures 7.5.8 and 7.5.9). Consequently a monostable pulse length of 0.2 ms is sufficient to allow the detector pulse to develop to its full amplitude. Once again a distortion has developed on the low energy side which is most likely a pulse pile up effect. The peak shown in figure 7.5.9 has a much sharper sloping edge on the high energy side than the peak shown in figure 7.5.8.

The following figures show some of the differential pulse height distributions.
obtained for 3.182787(24) MeV α-particles corresponding to various operating voltages together with the calibration pulse spectra. The results were repeatable. The gas used was always P-10 at a pressure of 758.5 torr at 0°C and the W value used to determine the gas gains was 26.0 eV/ip ± 0.5 eV/ip[1].

**ALPHA PARTICLES**

operating voltage = +1300 volts
monostable pulse length = 0.2 ms
time = 1k seconds
counts between channel 248 and 485 = 68162 cts
linear amplifier input attenuator = 1
time = 100 seconds
counts between channel 399 and 429 = 5011
test pulse amplitude = 0.376 volts
gas gain = 21.66±1.40

Figure 7.5.10
The differential pulse height distribution for 3.182787(24) MeV α-particles at an operating voltage of +1300 volts and the test pulse spectrum. The gas gain as determined by the pulse matching method was 21.66 ± 1.40. Current comparison give a value of 23.01 ± 1.47.
The differential pulse height distribution for 3.182787(24) MeV α-particles at an operating voltage of +1400 volts, and the test pulse spectrum. The gas gain obtained by the pulse matching method was $36.01 \pm 2.34$. Current comparisons give a value of $39.81 \pm 2.55$. 

Figure 7.5.11
The differential pulse height distribution for 3.182787(24) MeV α-particles at an operating voltage of +1500 volts and the test pulse spectrum. The gas gain obtained by the pulse matching method was 63.15 ± 4.10. Current comparisons give a value of 68.96 ± 4.41.
The differential pulse height distribution for 3.182787(24) MeV α-particles at an operating voltage of +1600 volts and the test pulse spectrum. The gas gain obtained by the pulse matching method was $112.35 \pm 7.29$. Current comparisons give a value of $124.83 \pm 7.99$. 

Figure 7.5.13
The differential pulse height distribution for 3.182787 MeV α-particles at an operating voltage of +1700 volts and the test pulse spectrum. The gas gain obtained by the pulse matching method was 210.29 ± 13.64. Current comparisons give a value of 228.77 ± 14.64.

In the above figures (see Figures 7.5.10 - 7.5.14) the test pulse peaks used to calculate the gas gains were a fraction of a percent FWHM. A summary of the results obtained by the test pulse method is given in figure 7.5.1.
Table 7.5.1
The results obtained by the pulse matching method compared with the results obtained by the current comparison method using the same detector, radiation source and gas filling. Within the experimental errors the results are in agreement.

The current comparison and pulse matching results shown above were obtained using the same detector, same radiation source and same gas filling. The value of the gas gains determined by current comparisons were always larger than those determined by pulse matching, this is indicated in the last column of Table 7.5.1 by the + sign and indicates the presence of a systematic error.

### 7.6 Conclusion

Previous authors using pulse matching methods have either shaped their pulse generator pulses to the same shape as their detector pulses or they have determined calibration factors to correct for the difference in pulse shapes (see chapter 6). Both of these approaches assume that the proportional counter pulses are always the same shape. This assumption is probably valid for electrons of $<10$ keV in heavy noble gases but for high energy electrons the shapes of the pulses will depend upon the orientation of the ionization tracks formed by the primary ionization. The methods discussed in chapter 6 also assume that all the positive charge is formed in the vicinity of the anode. This assumption will only be true for gas gains greater than $\sim 10$. With the method I have developed both the shapes of the detector and pulse generator pulses become irrelevant although it is necessary for the pulse generator pulses to be rectangular so their precise amplitudes at the moment the cathode is shorted are known.

The pulse matching method by shorting the cathode gave results which agreed with current comparison measurements performed on the same detector with the same gas filling and the same radiation source.
The accuracy of the pulse matching method using circuits similar to the circuit I have constructed may ultimately depend only on the precision to which the capacitance of the test capacitor, the volts function on the electrometer, the $W$-value, and the energy lost in the detector are known. With the above circuit the pulses had to be large before reliable results were obtained. In fact only for 3.2 MeV $\alpha$-particles at a gas gain of 20 were reliable results obtained. Since a 3.2 MeV $\alpha$-particle releases $1.2 \times 10^5$ ion pairs in P-10 (W-value 26.0 eV/ip) and the central capacitance of the system was $\approx 75$ pF, the pulses at the input of the circuit at a gas gain of 20 were $\approx 5.11 \times 10^{-3}$ volts. If the circuit is to be useful it will have to be more sensitive. It may be possible to improve the circuit by taking the pulse which closes the switch (HEF 4016B) from the central wire.

Alpha particles are not really suitable for the study of gas gain since so much charge is formed by the absorption of an $\alpha$-particle the resulting pulse may be affected by intrinsic space charge effects giving smaller values for the gas gain than would be obtained by using x-rays or electrons to produce the primary ionization. X-rays or electrons would, of course, produce much smaller pulses so the circuit would need to be more sensitive. Gas gains of less than 20 are also of interest and should be studied.

All the other results presented in this thesis were obtained by the current comparison method using x-rays or $\gamma$ rays.

References

8.1 Gas gain and the reduced field strength

It was suggested by Zastawny in 1966 [1] that the gas gain of a cylindrical proportional counter operating in the proportional region will be a function only of the reduced field strength at the surface of the anode.

In the electron avalanche the increase in the initial number of ion pairs, \( n \), is given by \( dn = n \alpha dr \), where \( \alpha \) is the first Townsend coefficient, and \( r \) is the distance from the axis of the detector. The first Townsend coefficient is defined as the number of ion pairs produced per unit path length by an electron moving under the influence of an electric field and therefore in the opposite direction to the field. It follows that the reciprocal of the first Townsend coefficient should be the mean path for ionization. It has been shown experimentally that \( \alpha/N \) is a function only of the reduced field strength \( E/N \) where \( N \) is the molecular number density and \( E \) the electric field strength [2].

The gas gain, \( G \) is given by

\[
\ln G = \int_{a}^{c} \alpha \, dr \quad (1)
\]

where \( a \) is the anode radius and \( c \) the radius at which gas gain begins. An electron moving in equilibrium with the field may not have gained all its energy in the last mean free path but may have gained and lost energy in collisions over several mean free paths before actually ionizing a gas atom. Over these several mean free paths the probability of ionization would have remained constant. The radius \( c \) would correspond to a distance from the central axis of the detector of one mean path for ionization plus the radius of the anode wire when the gas gain just equals two. When the radius of the anode wire is the same as \( c \), \( G = 1 \) and \( \ln G = 0 \), if \( c \) is greater than the anode wire radius \( G \) will always be greater than 1.

In a cylindrical proportional counter the field strength is given by
where \( V \) is the operating voltage, \( r \) the distance from the central axis of the detector, \( b \) the cathode radius and \( a \) the anode radius. Following the notation of Zastawny [1] and Aoyama [3] the reduced field strength is given by

\[
S = \frac{E}{N} = \frac{V}{rN \ln \left( \frac{b}{a} \right)}
\]

where \( S_a \) is the reduced field strength at the surface of the anode. Therefore, changing variables in equation (1) using equation (3), we have

\[
\ln G = - \int_{S_a}^{S_c} \frac{\alpha a S_a}{S^2} dS
\]

where \( S_c \) is the reduced field strength at the onset of gas gain. Therefore

\[
\frac{\ln G}{N} = - \int_{S_a}^{S_c} \frac{\alpha N}{a S_a} dS
\]

and since \( \alpha/N \) is a function of the reduced field strength

\[
\frac{\ln G}{Na S_a} = \int_{S_a}^{S_c} \frac{\alpha}{N} dS
\]

(4)

If \( S_c \) is a constant for a given gas or mixture of gases we have

\[
\frac{\ln G}{Na S_a} = f(S_a)
\]

(5)

Thus if the gas gain is measured for a range of detector parameters e.g. gas density, anode radius, a graph of \( \ln G/Na S_a \) against \( S_a \) should yield the same function.

Zastawny verified this for proportional counters filled with \( \text{CO}_2 \) by measuring the gas gain at four different gas densities [1]. He was also able to show that it held for P-10 (90% Ar plus 10% \( \text{CH}_4 \)) by using the data obtained by Williams and Sara [4]. According to Zastawny these authors had kept the gas density
constant but varied the anode radius [4].

Equation (5) was verified for nitrogen and xenon by obtaining values of gas gain for a range of gas densities.

8.2 Experimental results for nitrogen

Data for nitrogen was obtained at three different gas densities. These data are shown below in Figure 8.2.1

![Figure 8.2.1](image)

Figure 8.2.1
A plot of \( \ln(G)/(NaS_a) \) against \( S_a \) for nitrogen. The molecular number densities used to obtain the gas gains were 2.56x\(10^25\) m\(^{-3}\), 1.62x\(10^{25}\) m\(^{-3}\) and 6.51x\(10^{24}\) m\(^{-3}\).

The above plot of \( \ln(G)/(NaS_a) \) against \( S_a \) for nitrogen at three different densities verifies equation (5) for nitrogen. The points for the measurements at the different densities show virtually no scatter, sitting directly on top of each other.
The readings for the gas gains at the different densities were carried out successively, first the gas gains at the higher density were recorded and then the gas density was reduced and new gas gain measurements recorded and so on for three different gas densities. The gas gains for a particular gas density were, of course, recorded at the one sitting but several days elapsed before the gas density was reduced for the next set of readings. Overall the readings were recorded over a period of about four weeks. Since the same gas (at different densities) was being used to obtain the values any impurities present would remain constant. This probably helps to explain the absence of scatter in the values.

8.3 Experimental results for xenon

Data for xenon at two molecular number densities are shown in Figure 8.3.1.

![Figure 8.3.1](image)

**Figure 8.3.1**

A plot of \((\ln G)/(NaS_a)\) against \(S_a\) for xenon. The molecular number densities were \(7.03 \times 10^{24} \text{ m}^{-3}\) and \(2.68 \times 10^{25} \text{ m}^{-3}\).
The results for each density were collected on two different occasions about five months apart and are for two different xenon fillings, i.e. the detector was evacuated and refilled. The range of gas gains for the high density filling are from $\sim 1.01$ to 732 and for the low density filling $\sim 1.1$ to 2272 but since reduced field strength is $E/N$ the high molecular number density results cover a much smaller range of reduced field strengths. The results shown in Figure 8.3.1 once again confirm equation (5).

It seems possible to determine the reduced field strength for the onset of gas gain by extrapolating the function in Figure 8.3.1 to $(\ln G)/(NaS_a) = 0$. The best set of results to use would be those taken for the highest molecular number density because these results would have the largest gas gains for the lowest values of the reduced field strengths at the surface of the anode. The highest gas density shown in Figure 8.3.1 is $2.68 \times 10^{25}$ m$^{-3}$ and gas gains as low as 1.01, 1.1 and 1.3 were measured for this gas density.
Figure 8.3.2
The value for $S_c$, the reduced field strength for the onset of gas gain can be determined by extrapolating $F(S_a)$ to point where $\ln G = 0$. This value for the above set of results is $\sim 6 \times 10^{-20}$ Vm$^2$.

Figure 8.3.2 shows $\ln G/NaS_a$ vs $S_a$ for xenon at a molecular number density of $2.68 \times 10^{25}$ m$^{-3}$. If the results are extrapolated to $\ln G = 0$ they intercept the $S_a$ axis at approximately $6 \times 10^{-20}$ Vm$^2$. This gives a rough estimate for the reduced field strength at the onset of gas gain.

A naive model of an electron avalanche would consist of a single electron eventually gaining enough energy from the electric field to ionize a gas atom or molecule, losing all its energy in the impact, then both electrons starting from rest gaining enough energy in one mean path to ionize two gas atom or molecules and so on. If the value of $\sim 6 \times 10^{-20}$ Vm$^2$ for the onset of gas gain is reliable, then using detector 1 with xenon at a molecular number density of $\sim 7.03 \times 10^{24}$ m$^{-3}$ (199 torr at 0°C) and an operating voltage of 400 volts the gas gain has a
value of 2.2, i.e. ~ 2. A gas gain of ~ 2 means that one mean path for ionization exists between the point where the reduced field strength is ~ 6x10^{-20} \text{ Vm}^2 and the surface of the anode. At an operating voltage of 400 volts, S_a has the value of 2.59x10^{-19} \text{ Vm}^2 and the point with reduced field strength ~ 6x10^{-20} \text{ Vm}^2, i.e. S_c is at a distance of 1.51x10^{-4} \text{ m} from the central axis of the detector. This implies that the mean path for ionization is 1.16x10^{-4} \text{ m} or 0.116 \text{ mm}.

A gas gain of 3.79, i.e. ~ 4 occurs for an operating voltage of 500 volts. A gas gain of 4 would mean two mean paths for ionization. At 500 volts the value of S_a has increased to 3.23x10^{-19} \text{ Vm}^2. The point at which S_c occurs has now moved outward from the central axis of the detector a distance of 1.88x10^{-4} \text{ m} or 0.188 \text{ mm}. This would make the second mean path for ionization 3.7x10^{-5} \text{ m} or 0.037 \text{ mm}. Consequently the mean path for ionization grows progressively shorter as the avalanche develops.

At an operating voltage of 1,200 volts the electron avalanche must begin at a distance of about 12.9 anode radii from the axis of the detector or ~ 4.2x10^{-4} \text{ m} from the anode. The gas gain at this operating voltage is 2272 which means that about eleven mean paths for ionization must exist in that ~ 4.2x10^{-4} \text{ m}. The first mean path will be the largest with each successive mean path being progressively smaller. The large size of the first mean path for ionization suggests that the conditions for the Furry distribution exist (see chapter 1) in the initial stages of the electron avalanche.

Half of all the charge is created in the last mean path for ionization, so if we take a certain sized avalanche (or gas gain) then increase the voltage so that the avalanche (or gas gain) doubles in size it should be possible to calculate the mean path for ionization that produced half of the charge. At an operating voltage of 600 V the gas gain (with N = 7.03x10^{24} \text{ m}^{-3}) is 7.44 and at 700 V the gas gain has increased to 15.94. This gives a mean path for the formation of half the charge in the avalanche of about 5.8x10^{-6} \text{ m}. This implies an ionization cross section for xenon of 2.45x10^{-20} \text{ m}^2. If an electron starts from rest a distance of 5.8x10^{-6} \text{ m} from the anode it will gain 17.2 eV from the field before striking the anode. Hayashi gives the ionization cross section for xenon at 20 eV as 2.28x10^{-20} \text{ m}^2 [5] which agrees well with the above calculations.

**8.4 Conclusion**

The results for nitrogen and xenon presented in this chapter indicate that for these two gases the gas gain is a function only of the reduced field strength at the surface of the anode. Zastawny presented experimental results for CO_2 in 1966 also verifying this relationship. This means that equation (5) has been verified
for atomic and molecular gases with both two and three atoms. It seems reasonable to assume that it holds for all gases.

References

9.1 Introduction
In designing a proportional counter for a particular task it would be useful to be able to predict its characteristics from its geometry, operating voltage or fill gas density. The object of this chapter is to show that an equation proposed by Aoyama seems to do this satisfactorily for xenon over a wide range of densities. In chapter 8 it was shown experimentally that the gas gain of a proportional counter is a function only of the reduced field strength at the surface of the anode

\[ \ln G_{NaS_a} = \int_{S_e}^{s_a} \frac{\alpha}{N} \frac{dS}{S^2} \]  

The various formulae proposed for the purpose of predicting gas gain vary only in the form of \( \alpha/N \), which has been shown experimentally to be a function only of \( E/N \). A typical curve of \( \alpha/N \) vs \( E/N \) is given in Figure 9.1.1 below.

---

**Figure 9.1.1**
A typical graph of \( \alpha/N \) vs \( E/N \), taken from Charles [1].

The curve shown in Figure 9.1.1 above consists of an initial exponential rise followed by a linear region and then a region where the graph turns over.
Consider Figure 9.1.1, Diethorns form would describe a straight line through the origin and tangential to point c, and so should fit over a very limited range of reduced field strengths. Zastawny's form would fit the curve over the region b-c. Charles' form would fit the curve over a much wider range of reduced field strengths from b through to d.

The fact that the proposed forms of $\alpha/N$ listed in Table 9.1.1 fit the curve shown in Figure 9.1.1 in some regions explains to some extent how the various authors were able to obtain data to support their models. In addition to being partly correct in their forms for $\alpha/N$ the previous authors usually had poor data. Charles [1] has shown that the pulse matching method most often used to obtain the data can be out by as much as a factor of 10 if the difference in pulse shape of the detector and test pulses is not taken into account. Most authors did not consider this.

### 9.2 Aoyama's equation

Aoyama [2] has proposed that $\alpha/N$ can be expressed in terms of the reduced field strength as $KA^m\exp(-L/S^{1-m})$ where $K$, $L$ and $m$ are constants characteristic of the gas. The value of $m$ must lie between 0 and 1. He shows that the forms of $\alpha/N$ proposed by other authors are just special cases of his form. For example if $m = 1/2$ his form reduces to a combination of Rose and Korff's and Charles. If $m = 0$ Aoyama's form reduces to that of Williams and Sara and if $m = 1$ it reduces to that of Diethorn.

Aoyama arrived at his form for $\alpha/N$ from theoretical considerations. The first Townsend coefficient $\alpha$ can be expressed in the following way;

$$\alpha = \left(\frac{\text{number of mean free paths in the field direction}}{\text{the probability of a mean free path being larger than the mean free path for ionization}}\right)$$
where $\lambda_\tau$ is a mean free path in the field direction and $\lambda_i$ is the mean free path for ionization.

At any radius $r_1$ from the axis of the counter

$$e\int_{r_1}^{r_1+\lambda_i} E \, dr + \varepsilon_0 = V_i$$

where $\varepsilon_0$ is the initial electron energy, $e$ the electronic charge and $V_i$ the ionization potential of the gas.

After electron impact if the electron loses all its energy or is scattered isotropically the average value of $\varepsilon_0$ will be zero. If the electron has a tendency to be scattered in the forward direction it will be greater than zero. The electric field strength in the proportional counter at the radius $r$ is given by

$$E = \frac{V}{r \ln\left(\frac{b}{a}\right)}$$

where $V$ is the operating voltage, $b$ the cathode radius and $a$ the anode radius. If we assume that after an ionizing collision the electron is scattered isotropically and therefore $\varepsilon_0 = 0$ and combine (3) and (4) we obtain

$$e\int_{r_1}^{r_1+\lambda_i} \frac{V}{r \ln\left(\frac{b}{a}\right)} \, dr = eV_i$$

$$V \ln\left(\frac{r_1 + \lambda_i}{r_1}\right) = V_i$$

$$\ln\left(\frac{r_1 + \lambda_i}{r_1}\right) = \frac{V_i \ln\left(\frac{b}{a}\right)}{V}$$

Hence the ratio of the field strengths at points separated by a radial distance $\lambda_i$ is using (4) and (5)

$$R = \frac{E(r_1)}{E(r_1 + \lambda_i)} = \exp\left\{\frac{V_i \ln\left(\frac{b}{a}\right)}{V}\right\}$$

This equation is very useful because it gives a value for the change in field.
strength over the mean free path for ionization, \( \lambda_i \). For instance for detector 1 filled with xenon to a pressure of 198.84 torr at 0°C a gas gain of 2271.8 is obtained at an operating voltage of 1200 volts. Using equation (6)

\[
R = \exp \left\{ \frac{V_i}{V} \ln \left( \frac{b}{a} \right) \right\}
\]

\[
= \exp \left\{ \frac{12.13}{1200} \ln \left( \frac{1.9}{3.495 \times 10^{-3}} \right) \right\}
\]

\[
= 1.066
\]

This means that over one mean free path for ionization the field only deviates from being a uniform field by 6.6%. Under these conditions the field can be considered uniform over a \( \lambda_i \) interval. Therefore we can say that;

\[
\lambda_i = \frac{V_i}{E} \quad (7)
\]

Now substituting (7) in (2) we have for the first Townsend coefficient

\[
\alpha = \frac{1}{\lambda} \exp \left( -\frac{V_i}{\lambda E} \right) \quad (8)
\]

The relationship between mean free path and cross section is given by

\[
\lambda = \frac{1}{N \sigma} \quad (9)
\]

where \( \sigma \) is the collision cross section or

\[
\lambda = \frac{1}{hN \sigma} \quad (9)
\]

where \( h \) is a small dimensionless constant. Substituting (9) in (8) we obtain.

\[
\frac{\alpha}{N} = h \sigma \exp \left( -\frac{h \sigma V_i}{S} \right) \quad (10)
\]

The collision cross section for electrons is in fact a function of energy. All that is now required is the relationship between \( \sigma \) and \( S \). Since this will be unknown we assume

\[
\sigma = CS^m \quad (11)
\]

where \( C \) and \( m \) are constants depending upon the gas and the values of \( S \), the reduced field strength over which the counter is operating.

Substituting equation (11) into equation (10) we obtain;

\[
\frac{\alpha}{N} = hCS^m \exp \left( -\frac{hCS^m V_i}{S} \right)
\]

Amalgamating some of the constants gives;

\[
\frac{\alpha}{N} = KS^m \exp \left( \frac{L}{S^{1-m}} \right) \quad (12)
\]

where \( K = hC \) and \( L = hCV_i = KV_i \). Recalling equation (1) we have
Substituting equation (12) into equation (1) gives:

\[ \frac{\ln G}{NaS_a} = \int_{s_c}^{s_a} \alpha \left( \frac{L}{S^{m-1}} \right) dS \]

which is very simple to integrate.

\[ \frac{\ln G}{NaS_a} = \int_{s_c}^{s_a} K \exp \left( -LS^{m-1} \right) dS^{m-2} \]

Now

\[ S^{m-2} dS = \frac{dS^{m-1}}{m-1} \]

Hence

\[ \frac{\ln G}{NaS_a} = \int_{s_c}^{s_a} K \exp \left( -LS^{m-1} \right) dS^{m-1} \]

\[ = \left( -\frac{K}{L(m-1)} \exp \left( -LS^{m-1} \right) \right)_{s_c}^{s_a} \]

\[ \frac{\ln G}{NaS_a} = -\frac{K}{L(m-1)} \exp \left( -LS^{m-1}_a \right) + \frac{K}{L(m-1)} \exp \left( -LS^{m-1}_c \right) \]

\[ = \frac{1}{1-m} \frac{1}{V_i} \exp \left( -LS^{m-1}_a \right) - \frac{1}{m-1} \frac{1}{V_i} \exp \left( -LS^{m-1}_c \right) \]

The term in the second bracket containing \( S_c \) can be ignored because \( S_c \) will always be much smaller than \( S_a \) in normal proportional counter operation.

\[ \frac{\ln G}{NaS_a} = \left( \frac{1}{1-m} \frac{1}{V_i} \right) \exp \left( -LS^{m-1}_a \right) \]

Therefore expressing the equation in a form that should yield a straight line gives:

\[ \ln \left( \frac{\ln G}{NaS_a} \right) = -LS^{m-1}_a - M \quad (13) \]
where \( M = \ln \{(1-m)V_i\} \).

Kowalski [3] has determined the values of \( K, L \) and \( m \) for argon, krypton and xenon and a range of gas mixtures consisting of these noble gases with various organic and inorganic additives. The values he obtained for xenon are \( 3.9666 \times 10^{-12} \text{ [Vm}^2\text{]}^{0.580} \text{[eV]}^{-1}, 4.2048 \times 10^{-11} \text{ [Vm}^2\text{]}^{0.580}, \) and 0.420 for \( K, L \) and \( m \) respectively. Using Kowalski's value for \( m \) and Aoyama's equation (equation (13)) I have been able to obtain excellent fits with my gas gain measurements for xenon.

\[
\begin{align*}
\text{Figure 9.2.1} \\
\text{A fit of data obtained at a pressure of 198.9 torr at 0°C of xenon to Aoyama's equation.}
\end{align*}
\]

The data for xenon at a pressure of 198.8 torr at 0°C fits Aoyama's equation very well (see Figure 9.2.1). Kowalski's value for the constant \( m \) appears to be accurate. The equation holds for gas gains ranging from 1.45 to 2271.83. At very high gas gains electron multiplication may not be proceeding by electron impact which might explain why the two points at high gas gains show a departure from the straight line. The points that do not lie on the line at low gas
gains are for gas gains of only 1.10 and 1.23 and at these gas gain it may not be valid to assume that $S_c$ is large compared with $S_a$.

Over the range of gas gains for which the equation holds (i.e. $-1.4$ to $-2300$) the correlation coefficient is 0.9999. The two points at large gas gains which lie above the line are values of gas gain of 11061.34 and 4777493. The values obtained for the constants are

$$ L = 4.17 \times 10^{-11} \text{ [V m}^2\text{]}^{0.580} $$

and

$$ V_i = 11.26 \text{ eV.} $$

in close agreement with Kowalski's values[3].

The ionization potential for xenon is 12.13 eV so the value of $V_i$ is out by 0.87 eV. This means that the value for $\epsilon_0$ in equation (3) is not zero as assumed. Aoyama found a similar effect for P-10 which he attributes to scattering in the forward direction rather than isotropic scattering[2].

I have also obtained data which verifies Aoyama's equation at pressures of $\sim 1$ atm, these results are shown in Figure 9.2.2.
Figure 9.2.2
Aoyama's equation fitted to data obtained at a xenon gas pressure of 757.5 torr at 0°C.

The constants for the results shown in Figure 9.2.2 are

\[ V_1 = 10.95 \text{ eV} \]
\[ L = 4.13 \times 10^{-11} \text{ [Vm}^2]\text{]^{0.580}} \]

A curve of \( \alpha/N \) vs. S can be obtained using the values derived from the data presented in Figure 9.2.1 or Figure 9.2.2. This is shown in Figure 9.2.3 in which equation (11) is plotted using the values of K and L obtained from Figure 9.2.1 and taking Kowalski's value of m, i.e. m=0.420.
Figure 9.2.3
The reduced first Townsend coefficient $\alpha/N$ as a function of the reduced field strength. The values of $\alpha/N$ were calculated from the constants derived from the experimental results used to obtain the data for Figure 9.2.1. The range of the values of $S$ were chosen to correspond to the reduced field strengths at the surface of the anode using detector 1 with a gas filling of xenon at 200 torr at $0^\circ$C for operating voltages from 0 volts to 1200 volts.

9.3 Conclusion

Aoyama's equation seems to be a good description of gas gain in proportional counters provided ionization proceeds by electron impact and the variation in field strength over a mean free path for ionization in the region of the electron avalanche is small enough for the field to be approximated to a uniform field.
References

10.1 Introduction

Experiments were performed using 2,3 dimethyl-2-butene (DMB) as an additive to xenon and it was found that at certain concentrations of additive dramatic increases in gas gain occurred.

In a proportional counter containing xenon (ionization potential 12.13 eV) the amount of ionization produced for a given particle energy loss or for a given operating voltage may be increased by using an additive whose ionization potential is lower than the excited states of xenon. For example, in the primary ionization and also in the electron avalanche the energy contained in the xenon metastable states may be transferred to the additive in collisions, resulting in the ionization of the additive (the Penning effect). The increased ionization would be expected to result in larger pulses and improved energy resolution [1] depending upon the geometry of the chamber and the gas gains used [2,3].

With polyatomic additives the Penning effect may not necessarily occur since there are other inelastic channels in addition to Penning ionization (PI). The bond energies of the C=C and C-H bonds are only 3.6 and 4.3 eV respectively so, of course, a hydrocarbon can break up into free radicals as an alternative to PI and there are other inelastic channels as well [4].

I chose 2,3 dimethyl-2-butene as an additive because its published ionization potential of (8.30 ± 0.02) eV [5] is just below the lowest excited state of xenon which is (8.315 ± 0.010) eV [6].

10.2 Experiment

Detector 1 was used for these experiments (see Chapter 2). The experiments were carried out at three different molecular number densities, 2.7x10^{25} m^{-3} (~1 atm), 1.4x10^{25} m^{-3} (~0.5 atm) and 7.0x10^{24} m^{-3} (~0.26 atm).

At low gas density (~7.0x10^{24} m^{-3}) absolute values of the gas gains were
determined using the electrometer to obtain current-voltage characteristic curves as in Figure 10.3.1. Guard rings prevented leakage currents between cathode and anode (see Chapter 2). The experiments were carried out using an $^{55}$Fe source and the central beryllium window for low gas gains, and a radium source for large gas gains in order to reduce space charge effects. When the current rose towards $\sim 10^{-10}$ A in the low gas gain region, the count rate was reduced to minimize space charge effects and increase the accuracy of measurements. The radium source required no beryllium window and irradiated the detector along its entire length so that avalanches were not confined to a small section of the anode. A density of $\sim 7.0 \times 10^{24}$ m$^{-3}$ was chosen to allow absorption of the x-rays (5.9 keV) across the whole diameter of the counter instead of near the counter window, giving good charge collection in the ion chamber region. The DMB was placed in a sample tube attached to a vacuum system, frozen and pumped to remove air, then released into a flask containing sodium to remove water vapour and from there introduced to the detector. The pressure of the DMB vapour was measured to be 76.5 torr at room temperature ($24^\circ$C). The detector was then filled with xenon to the required density. The mixtures ranged from 35.12% DMB down to pure xenon.

The higher density experiments were performed using the radium source because it was found that a good ion saturation curve could not be obtained with the $^{55}$Fe source (see Chapter 4). The use of radium gave a more uniform absorption of $\gamma$-rays throughout the volume of the detector. To reduce the number of observations and speed up the experiment, the ion saturation current was determined by reversing the polarity of the electrodes and measuring the current at a high voltage to ensure complete charge collection.

The range of mixtures for the $2.7 \times 10^{25}$ m$^{-3}$ density fillings was from 1.26% down to pure xenon, and in the case of the $1.4 \times 10^{25}$ m$^{-3}$ density fillings the range was from 1.33% to pure xenon. In all cases, the method of changing the concentration of additive consisted of removing some of the gas from the detector after each set of measurements and replacing it with pure xenon to obtain a new concentration of additive.

10.3 Results

Some of the results of the investigation are shown in the figures. Figure 10.3.1 shows the ionization current as a function of anode potential for pure xenon and for xenon plus 0.23% DMB, both curves being obtained for a gas density of $7.0 \times 10^{24}$ m$^{-3}$. 
Figure 10.3.1
The current measured as a function of absolute operating voltage for pure xenon and xenon+0.23%DMB, at low density (~ 0.26 atm). The central wire is the anode.

Figures 10.3.2, 10.3.3 and 10.3.4 show the gas gains as a function of additive for several different operating voltages for the three different densities used (2.7x10^25, 1.4x10^25 and 7.0x10^24 m^-3). Gas gains of more than 10^5 were obtained at operating voltages for which pure xenon exhibits a gas gain of order 10. These curves are for low percentages of the additive and show a rapid rise of gas gain for very small amounts of DMB and marked peaks in gas gain vs percentages of DMB, particularly for low gas density fillings.
Figure 10.3.2
The gas gain for mixtures at approximately 1 atm ranging from 1.26% DMB through to pure xenon.
Figure 10.3.3
The gas gains for mixtures at approximately 0.5 atm ranging from 1.33% through to pure xenon. As in Figure 11.3.2 the gas gain rises (from left to right) to a maximum at ~ 0.4% DMB concentration level.
Figure 10.3.4
The gas gains for mixtures at approximately 0.26 atm ranging from 1.06% additive through to pure xenon.

Figure 10.3.5 shows the gas gain at 600 V over the whole range of percentage of additive investigated for the low density case (7.0x10^{24} m^{-3}). At the peak (0.23% DMB), the gas gain is 461.5 compared with ~8 in pure xenon under identical conditions. To obtain a similar gas gain with pure xenon the anode potential has to be raised to ~1050 V.
The gas gain over the whole range of low density mixtures (~ 0.26 atm) tested. The peak represents a gas gain of about 460 at an anode potential of 600 V compared with a gas gain for pure xenon of about 8 at the same anode potential.

With the low density filling with ~ 0.2% DMB a good pulse height distribution is obtained at 600 V (FWHM ~ 16% at 5.9 keV). However, this is not appreciably different from the resolution obtained with conventional mixtures (e.g. Xe + CH₄). The relative variance of the gas gain at gas gains above ~ 10 would offset any beneficial effects of the additive on the resolution of the detector [1].

10.4 Discussion

The peaks in gas gain for the ~ 1 and ~ 0.5 atm mixtures have in common the rise from 0% DMB to a maximum at ~ 0.4% DMB suggesting that the same
process is operating at both gas densities in this region. As the concentration level is further increased the peak for the higher pressure mixtures is flat-topped whereas that for the ~ 0.5 atm mixtures is more rounded. When the pressure is ~ 0.26 atm the peak becomes much better defined and occurs at a lower DMB concentration level. The peaks shown in Figures 10.3.2, 10.3.3 and 10.3.4 are defined at gas gains of the order of $10^{5}$.

At a density of $2.7 \times 10^{25} \text{ m}^{-3} (~ 1 \text{ atm})$ (see Figure 10.3.2) the peak is flat-topped and there is no fall-off in gas gain until the concentration of DMB reaches approximately 0.75%. Two different mechanisms may be responsible for this peak: at higher concentrations of additive the nonmetastable Penning effect (NMPE) is operative [7,8] and at around 0.4% DMB the metastable Penning effect (MPE) is responsible for the increased ionization yield. The MPE is the increase in ionization due to collisions between xenon atoms in long-lived metastable states and DMB molecules. As noted earlier, the DMB molecule has an ionization potential lower than the lowest excited state of xenon and in the collisions the energy from the metastable states may be transferred to the DMB molecules. The NMPE is the ionization of the additive by collisions with xenon atoms excited to nonmetastable energy levels. These nonmetastable energy levels are shorter lived, and if the energy is to be transferred to the additive by collisions, a greater concentration of additive is needed. Under the conditions shown in Figure 10.3.2 the higher density xenon traps resonance photons from excited xenon atoms [9], extending the effective lifetimes of the excited xenon resonance states. For additive concentrations greater than about 0.4% these longer-lived nonmetastable states are able to transfer their energy to the DMB in collisions, thereby increasing the ionization yield within the detector. The DMB may also have the effect of lowering the electron temperature, so that as the DMB concentration is increased, larger anode potentials are required to achieve identical gas gains. This process would compete with the NMPE and as the concentration of additive increases above 0.75% the lowering of the electron temperature may be having the dominant effect and the gas gain begins to fall. If the concentration of additive is reduced the probability of ionization by nonmetastable states must also, and eventually the MPE must be the dominant process. At even lower concentrations of DMB the MPE becomes less significant and the gas gains fall toward the pure xenon values.

At a density of $1.4 \times 10^{25} \text{ m}^{-3}$ (see Figure 10.3.3) the peak is much sharper and reaches a maximum at ~ 0.43% DMB concentration. The reduced xenon density shortens the effective lifetimes of the metastable states in the xenon, diminishing the importance of the NMPE. The MPE must occur at all gas densities and the rise in gas gain from 0% DMB to about 0.4% DMB is common to both Figure 10.3.2 and Figure 10.3.3, so the peak shown in Figure 10.3.3 may be due
almost entirely to the MPE.

A different process may be responsible for the results shown in Figure 10.3.4 (representing the lowest gas density tested). At the position of the peak, the concentration of DMB is so low that there may be insufficient additive for the MPE to occur, and the metastable atoms then form vibrationally excited xenon molecules in three-body collisions which radiate UV photons of energy ~ 8.3 eV [10]. These molecules ionize the additive with great efficiency causing the very sharp peak at about 0.23% DMB. As the gas density increases so does the rate at which these molecules lose their vibrational excitation in two-body collisions [10]; vibrationally relaxed excited molecules are unable to ionize the DMB which could explain the absence of any features in Figure 10.3.2 and Figure 10.3.3 at the 0.2% DMB concentration level.

The above idea could be tested by separating the xenon from the DMB and observing whether or not avalanches in the xenon triggered avalanches in the DMB. This would require a detector with two anode wires and a UV transparent wall between the anode wires creating two compartments. The xenon density could be varied and the effects studied.

10.5 Conclusion

The addition of a small quantity of 2,3 dimethyl-2-butene to xenon results in peaks in gas gain, and the shape and position of these peaks depend upon the density of the detector filling. The increase in gain can easily be of the order of $10^4$ and one application is the operation of proportional counters at lower operating voltages than with conventional fillings like Xe + CO₂.

The above results were published in Nuclear Instruments and Methods in Physics Research [11]. All experimental measurements were made by K. G. White, Dr K. B. Fenton suggested using 2,3 dimethyl-2-butene as an additive, and Dr A. G. Fenton provided the additive in vapour form in a flask so that it could be attached to the gas filling manifold after removal of air and water vapour.

Experiments were also carried out using tetramethyltin (CH₃)₄Sn as an additive to xenon and the results obtained were similar to those obtained for DMB. Unfortunately there are some doubts concerning these results and consequently they have not been presented in this thesis.

References

11.1 Introduction

The W-value of a gas or mixture of gases is the mean energy expended to form an ion pair in the gas. If $E$ is the energy loss in the gas and $n_0$ the number of ion pairs formed in the gas then $W = \frac{E}{n_0}$. If there is a region in which the mean energy expended to produce an ion pair is a function of the energy $E$ it should be denoted by a different symbol, say $w(E)$.

Then the relationship between $W$ and $w(E)$ will be given by

$$ W = \frac{1}{E_{\text{max}} - E_{\text{min}}} \int_{E_{\text{min}}}^{E_{\text{max}}} w(E) \, dE $$  \hspace{1cm} (1)

Since $w(E)$ will increase asymptotically towards $+\infty$ as $E_{\text{min}}$ approaches the ionization potential of the gas or mixture of gases, $E_{\text{min}}$ must be chosen so that the above integral converges. If $w(E)$ is a constant, equation (1) reduces to $W = w$ [1].

For the gases used in proportional counters $W$ seems to be independent of energy or these detectors would not be proportional.

As discussed in chapter 1 the energy resolution of a proportional counter, $R$, can be expressed as

$$ R = 2.35 \sqrt{\frac{(F + f) \, W}{E}} $$  \hspace{1cm} (2)

where $F$ is the Fano factor and $f$ the relative variance of the gas gain [2]. The energy resolution is normally expressed as a percentage FWHM. From equation (2) it can be seen that a reduction in $W$ should result in an improvement in energy resolution provided the other constants remain the same. In practice $f$ tends to dominate the above expression but it should be possible to improve the energy resolution of a proportional counter by lowering the $W$-value provided low gas gains are used [2] or the electric field in the region of the electron avalanches is uniform[3].
11.2 The W-values for xenon

Only the W-values for electrons in xenon will be considered. Since xenon filled proportional counters seem to be proportional the W-value should be constant independent of energy. W-values for xenon widely accepted in the literature are $21.9 \pm 0.3$ [4] and $21.5 \pm 0.4$ eV/ip [5]. Combecher [6] has obtained results which show an energy dependence for low energy electrons and these results are given in Figure 11.2.1. According to Combecher, even at 1 keV the w-value for electrons in xenon has risen to 23.78 eV/ip [6].

![Figure 11.2.1](image)

**Figure 11.2.1**
The energy dependence of the w-value for low energy electrons in xenon. The measurements were taken from Combecher [6] and are accurate to within 2%.

11.3 Experimental results using xenon plus DMB mixtures

I measured the W-values of xenon plus DMB mixtures for concentrations of DMB ranging from 35.11% DMB through to pure xenon. These measurements
were made using $^{55}$Fe and detector 1. The technique consisted of measuring the ionisation current due to the source and then measuring the count rate from the source. The $W$-value is then given by

$$W = \frac{N Fe}{i_s} \quad (3)$$

where $N$ is the count rate, $E$ is the energy absorbed by the gas, $e$ the electronic charge and $i_s$ the ion saturation current.

I obtained the ion saturation currents by reversing the polarity of the electrodes so that the central wire became the cathode. The operating voltage was made high ~ 700 - 1000 volts to ensure complete charge collection occurred. The charge carriers for the positive charges in these gas mixtures would have been the DMB molecules because of their lower ionisation potential (8.30 eV [7]) compared with xenon (12.13 eV). The positively charged xenon ions would have transferred their positive charges to the DMB molecules in collisions. A DMB molecule neutralizing itself at the cathode would either dissociate or absorb the excess energy in radiationless transitions. Because of this absence of secondary electron production at the cathode, reversing the polarity of the electrodes and using the central wire as the cathode should permit complete charge collection without gas gain and with no secondary currents.

The background current, probably due to contact potential differences (see chapter 2) was recorded first and then the source was put in place and the ionisation current was recorded. The current due to the source could then be determined by subtracting the current due to the background. The source was left in place and a differential pulse height distribution was obtained by operating the detector as a proportional counter. The source was then removed and the background count rate was recorded and subtracted from the previous spectrum due to the source plus background. The values obtained were then substituted into equation (3) to obtain the value for $W$. The $W$ values obtained for xenon seem to suggest that the results might be more accurate than the error bars on the graphs indicate.
The W-values for xenon plus DMB for mixtures ranging from 35.11\% through to pure xenon. The total gas pressure for each mixture was kept constant at \( \sim 200 \) torr at 0\(^\circ\)C.

Figure 11.3.1 shows the results obtained for mixtures ranging from 35.11\% through to pure xenon. The large errors on the values make it difficult to determine if the Penning effect (discussed in chapter 1) is occurring but there does seem to be a trend in the results suggesting that it may be occurring.

Figure 11.3.2 show the results for mixtures ranging from \( \sim 4.9\% \) DMB to pure xenon on an expanded scale.
11.3.2

The W-values for mixtures of xenon plus DMB from ~ 4.9% DMB through to pure xenon. The pressure of each mixture was kept constant at ~ 200 torr at 0°C and the radiation source was $^{55}$Fe.

The trend in the mean values of the results seems to indicate that the Penning effect may be occurring. Consequently the increases in gas gain reported for these mixtures might be due to the Penning effect [8]. The minimum in the mean values of the W-values and the maximum in the gas gains are approximately in the same position (see chapter 11).

11.4 Conclusion

The results I obtained for the W-values for xenon plus DMB mixtures seem to indicate that the Penning effect might occur to some extent in these mixtures. This means that the large gas gains reported for these mixtures may be due to the Penning effect as suggested in chapter 11 and reference [8].
The errors in the above measurements were due to the 5% accuracy in making current measurements with the Keithley electrometer. This problem could have been overcome by using two detectors, one detector containing the gas mixture under investigation and the other containing a reference gas or gas mixture with an accurately known W-value. The detectors should be initially operated in the proportional mode and the count rate from the $^{55}$Fe source or sources adjusted so that it is the same for both detectors. This can be accomplished by using Al absorbers, or by altering the distance between the counters and the sources. When the count rates are identical the counters should be operated in current mode and the ion saturation currents measured, the unknown W-value can then be determined from the ratio of the ion saturation currents and the known W-value of the reference mixture. Jarvinen and Sipila [9], using Ar-CO$_2$ as a reference mixture ($W = 26.0$ eV/ip), have measured the W-values of several gas mixtures using this technique.

References

12.1 Introduction

When detector 1 was filled with xenon plus large concentrations of DMB and operated using the $^{55}$Fe source at the central beryllium window particular ageing effects would occur. These consisted of a distortion of the full energy peak eventually leading to the development of a second peak.

The differential pulse height distribution shown below was obtained using xenon as the fill gas and $^{55}$Fe as the radiation source. Prior to this particular gas filling the detector had been in use over a long period of time with several different gas fillings.

![Differential Pulse Height Distribution](image)

**Figure 12.1.1**
The differential pulse height distribution for xenon at a pressure of 201.2 torr at 0°C using detector 1. The radiation source was $^{55}$Fe and the operating voltage was 1300 volts.

The spectrum shown above was obtained at a gas gain of ~4840 and the energy resolution was 24.45 % FWHM. The point of inflexion on the ion saturation curve was at ~50 volts. The above pulse height distribution has a distortion on the high energy side. The radiation source emits Mn $K_{\alpha}$ x-rays of ~5.9 keV and Mn $K_{\beta}$ x-rays of 6.49 keV. The energy resolution of the detector was 24.45 %
FWHM which means that two peaks have to be about 1.44 keV apart to be resolved, consequently the detector would not be expected to resolve the 6.49 keV x-rays. Considering that for every 20.3 Kα's the source emits 150.5 Kα's the spectrum should show a slight deviation from the gaussian shape. It will be shown that the distortion of the above spectrum (see Figure 12.1.1) on the high energy side is actually due to a build up of material on the anode.

The detector was evacuated and filled with a mixture of xenon plus 2,3 dimethyl-2-butene (DMB). The pressure of the DMB was 49 torr at 25.2°C and the final total pressure was 222 torr at 25.0°C or 203 torr at 0°C. The percentage of DMB was therefore 22%. This mixture gave an ion saturation curve with a point of inflexion at about 120 volts. The most interesting aspect of this gas filling is the differential pulse height distribution. The differential pulse height distribution is shown in Figure 12.1.2.

![Figure 12.1.2](image)

**Figure 12.1.2**
The differential pulse height distribution for xenon plus 22% DMB at a pressure of 203 torr at 0°C. The detector is detector 1 and the radiation source is 55Fe. The pulse height distribution was obtained at an operating voltage of 1500 volts.

The pulse height distribution for this particular gas mixture gave a curious second peak at what appeared to be twice the energy of the full energy peak. The count rate was only 126.4 counts per second so it is difficult to believe that the peak was the result of pulse pile up.

The concentration of DMB was reduced several times (keeping the total pressure constant) and for each mixture the differential pulse height distribution for 55Fe was recorded. Each pulse height distribution showed the extra peak. Detector 1
also had a beryllium window located in the cylindrical wall close to one end. This window was never used for the experimental work presented in this thesis (except when specifically mentioned) because the electric field might have been distorted by the proximity to the end. When the concentration of DMB had been reduced to 11.26 % the differential pulse height distributions from both windows were compared. The results are shown in Figure 12.1.3 below.

![Figure 12.1.3](image)

**Figure 12.1.3**
The pulse height distributions for the central and end windows for detector 1. The gas mixture is xenon plus 11.26 % DMB at a total pressure of 205 torr at 0°C. The radiation source is $^{55}$Fe and the operating voltage is 1200 volts.

As can be seen the double peak appears to be absent from the end window. The count rates are low for both pulse height distributions being 209.8 ± 0.5 cts per sec for the central window and 641.2 ± 0.8 cts for the end window.

The absence of a double peak at the end window is evidence that the double peak is not due to the gas or the radiation source since these are the same for both distributions. The differences must be due to a build up of material on the anode (central wire). The detector (detector 1) with the central wire used for most of the work described in this thesis had been in use for some time before any of the work described in this thesis had begun. The distortion of the full energy peak
shown in Figure 12.1.1 was probably the result of previous usage, not a result of the particular xenon filling and due to a build up of material on the anode. Large percentages of DMB appear to have caused a rapid growth in this build up. The two peaks in the pulse height distributions shown in Figures 12.1.2 and 12.1.3 are probably due to avalanches on one side of the anode undergoing a different gain to avalanches on the other side of the anode or elsewhere in the detector. The number of counts recorded in 1K seconds are 24522 for the peak in the highest energy position and 94257 counts for the other peak. The L escape peak has 7660 counts. The ratio of the sizes of the two full energy peaks is 3.84 and this corresponds to the ratio of the number of x - ray photons absorbed each side of the anode which is 3.70. The avalanche activity each side of the anode need not correspond to the ratio of the number of photons absorbed each side of the anode. For example, xenon has an L fluorescent yield of 0.23 [2] and if $^{55}$Fe is used the fluorescence photons will be more energetic than the photoelectrons and these photons can start avalanches elsewhere in the detector. Since the ratio of the sizes of the peaks closely corresponds to the ratio of x-rays absorbed each side of the anode then this ratio probably closely corresponds to the intensity of the avalanche activity. This also shows, for that particular percentage of DMB and under those operating conditions, that the avalanches do not spread around the circumference of the anode.

To remove this build up of material a current of ~ 800 mA was passed through the anode (central wire). The 22 % DMB mixture had been left in the detector. The process of "burning" the deposit off the anode or "flashing" the anode changed the properties of the gas so that it was not possible to obtain a full energy peak using the $^{55}$Fe source and the counter had to be evacuated. A current sufficient to cause the anode to glow red (500 mA) was once again passed through the anode while the detector was under vacuum. After considerable pumping the detector was filled with xenon to a pressure of 204 torr at 0°C. A full energy peak was obtained (see Figure 12.1.4 below) using the $^{55}$Fe source and there was no distortion on the high energy side. The energy resolution was ~ 17 % FWHM. It seems that the distortion in the pulse height distribution shown in Figure 12.1.1 was the result of a deposit on the anode.
12.2 Ageing experiments

In the first ageing experiment the detector was filled to a molecular number density of $7.28 \times 10^{24} \text{m}^{-3}$ (i.e. 206 torr at 0°C) with 27.14% DMB and 72.86% xenon. The operating voltage was 1400 volts giving a gas gain of about 2,500. This gas gain was measured at the conclusion of the ageing experiment so that it did not contribute to the ageing of the detector. The gas gain was measured by operating the detector in current mode rather than in pulse mode and comparing the current generated by the $^{55}$Fe count rate used for the experiment with the current obtained by reversing the polarity of the electrodes. The first current was measured with the central wire (the anode) at +1400 volts with respect to the cathode and the second with the central wire (now the cathode) at -1000 volts with respect to the anode. The background currents were subtracted so that an accurate gas gain for the source was obtained. The gas gain obtained from these measurements was adjusted for the change that had occurred in the position of the peak of the differential pulse height distribution during the ageing experiment. The fluorescent yield was approximately 0.057. The energy resolution was approximately 20% FWHM at 5.9 keV. The geometry of the situation is shown in Figure 12.2.1.
Detector dimensions:
outside diameter = 4.14 cm
inside diameter = 3.78 cm
wall thickness = 1.70 mm
beryllium window = 3 mm diameter
source diameter = 12.5 mm
source-window separation = 6 cm

Figure 12.2.1
A plan of the detector source geometry for the ageing experiment.

There was some collimation of the x-rays, the longest possible path length in the
gas being 3.83 cm and the shortest being 3.8 cm. The x-rays absorbed in Region
1 (see Figure 12.2.1) will result in avalanche activity on the side of the anode
facing the window and the x-rays absorbed in Region 2 will give rise to
avalanche activity on the side of the anode facing away from the window. In the
proportional region the avalanches are restricted to less than half the
circumference of the anode whilst in the semiproportional region the avalanches
are believed to completely surround the anode [1]. Very few avalanches will
approach the anode from a position perpendicular to the x-ray beam. Since the
intensity of an x-ray beam in xenon follows an exponential decrease with
distance more x-rays will be absorbed in Region 1 than in Region 2. Thus the
7.7 mm of the anode facing the window in the path of the beam will receive more
avalanches than the 12.4 mm of the anode facing away from the beam (see
Figure 12.2.1). Unfortunately this does not mean that avalanche activity will be
confined to the 7.7 mm and 12.4 mm regions of anode. The L fluorescent yield
of xenon is 0.23 [2] which means that 23% of all x-rays absorbed result in the
emission of characteristic x-rays as well as photoelectrons. The photoelectrons
and Auger electrons will have "ranges" of a fraction of a millimeter but the
characteristic x-rays will have large mean free paths for absorption in xenon and
will start electron avalanches far from the point of origin. The mean free paths
for absorption are roughly 30 mm [3]. Table 12.2.1 gives the energies and
relative intensities of these characteristic x-rays.
Fluorescence energy (keV) | $\text{La}_1$ | $\text{La}_2$ | $\text{L}_\beta_1$ | $\text{L}_\beta_2$ | $\text{L}_\beta_3$
---|---|---|---|---|---
4.093 | 4.094 | 4.403 | 4.58 | 4.498

Table 12.2.1

Xenon x-ray fluorescence lines and relative intensities after excitation by 5.9 keV x-rays taken from Gorenstein et al [2].

Most of the escape photons would originate from absorption events near the window, the energy left in the counter forming the pulses of the escape peak seen in the pulse height distribution.

The pressure of xenon at 0°C was 150.1 torr and the absorption coefficient of 6 keV x-rays in xenon is $6.69 \times 10^2$ cm$^2$/g; using this information $\sim 77\%$ of the photons will be absorbed in Region 1 and a further $\sim 77\%$ of the beam will be absorbed in Region 2. This means that 3.35 photons are absorbed in Region 1 for every photon that is absorbed in Region 2. Overall the beam will be attenuated by $\sim 99.5\%$. The weighted mean value of the Mn x-rays from the source is 5.97 keV [4] and the weighted mean value of the xenon L fluorescence x-rays is 4.25 keV, so if it is assumed that all the xenon fluorescence x-rays from Region 1 leave the region completely and start avalanches elsewhere, the energy left in Region 1 will have a mean value of 1.72 keV. Consequently $\sim 77\%$ of the beam will be absorbed in Region 1, 23% of these events will have an energy of 1.72 keV and the remainder will have an energy of 5.97 keV.

The observed ageing effects consist of a drop in gas gain followed by a distortion in the shape of the full energy peak and eventually the development of two peaks. Similar observations have been made in the past with regards to noble gas plus hydrocarbon mixtures [5,6,7,8]. These effects are widely held to be due to the build up of deposits on the anode. Experimental work has been performed by den Baggende et al [5] demonstrating that the twin peaks can be the result of uneven deposits on the anode. The gas gain of a proportional counter depends exponentially on the radius of the anode [9] consequently if this varies only slightly from one region to another, avalanches on these different regions will undergo different gas gains. In the case of detector 1 a greater build up of deposit on the portion of the anode facing the window would result in a lower gas gain for those avalanches reaching that part of the anode.

The ageing of proportional counters filled with noble gas/hydrocarbon mixtures has been shown to be function only of the total number of electrons arriving at the anode (or positive ions arriving at the cathode) [5]. The mean energy
expended to produce an ion pair (the W-value) in the xenon plus 27.14% DMB was determined to be approximately 25 eV (see chapter 12). The determination of the W-value was carried out using the same detector but a different gas filling of similar composition. A new gas filling was used for the ageing experiments. Each full energy pulse will be due to ~239 avalanches each resulting in the formation of ~2,500 electrons, consequently the pulse at the detector output will be due to ~596600 electrons. Similarly pulses due to an energy loss of 1.72 keV will result from 172,000 electrons collected at the anode. The total count rate was 12700 counts/sec, 77% of these are absorbed in Region 1 and 23% excite L fluorescence x-rays which will be assumed to have left Region 1. This gives about 6.34x10^9 electrons per second on the 7.7 mm of anode wire facing the beryllium window, or 8.23x10^8 electrons per second per mm of anode wire. It is assumed that the avalanche activity is uniform over this 7.7 mm of anode.

At the beginning of the experiment the full energy peak was centred on channel 123 and the energy resolution was 19.5% FWHM. After about 3 hours the peak had dropped to channel 116. The distribution had lost its symmetry after 9 hours and the peak had dropped to channel 106. The increasing distortion of the differential pulse height distribution with time is illustrated in Figure 13.2.2 below.
The counter was irradiated for a total of $\sim 4.76 \times 10^4$ seconds and during this time the full energy peak split up into two peaks with the larger of the two dropping in gain by $\sim 0.675$. It is assumed that the larger peak is due to a build up of material on the 7.7 mm of anode facing the source. The first signs of distortion in the differential pulse height distribution were seen after about $3.2 \times 10^4$ seconds or 8.88 hours. Taking 2,300 as the average gas gain over this period, the number of bombarding electrons would be $\sim 2.4 \times 10^{13}$ per mm of anode facing the entrance window. Figure 13.2.3 below shows the channel number as a function of time. After about 9 hours of irradiation the drop in height is constant at about 5.5 channels per hour.
Figure 12.2.3
The channel number of the full energy peak as a function of time for xenon plus 27.14% DMB.

At the conclusion of the experiment the ratio of the number of counts in the two full energy peaks was approximately 1.8:1. If it is assumed that the avalanche activity on the 7.7 mm of anode facing the beryllium window is responsible for the largest peak, and the smaller peak is due to avalanches caused by the absorption of xenon L fluorescence x-rays elsewhere in the counter and avalanche activity on the other side of the anode, then the ratio of the sizes of the two peaks should be 1.5:1. The discrepancy between the experimental and theoretical results may be due to the assumption that all the xenon L fluorescence x-rays originating in Region 1 cause avalanches elsewhere in the counter, some are certain to be absorbed in Region 1 contributing to the avalanche activity there. The source was off axis with the detector in the horizontal plane during this experiment but this does not appear to have affected the results. During the collection of the data presented in Figure 12.2.3 there was no attempt to
determine whether or not there was any drift in the electronics.

After about 15 hours of irradiation a current, large enough to cause the anode to glow red was passed through the anode. This current was measured to be \( \sim 0.885 \) A r.m.s., and the voltage across the anode required to produce this current was about 40 V r.m.s.. The pulse height distribution returned to normal with energy resolution of 19.5% FWHM. The centroid of the full energy peak occurred in channel 113 where previously it had occurred in channel 123. This could be due to an increase in the fill gas pressure as a result of outgassing from the anode or alternatively electronegative impurities may have been added by the heating process. A current of about 0.9 A r.m.s. was passed through the anode a second time and the centroid of the full energy peak moved to channel 105, the result of further outgassing.

Other authors [6] have used Diethorn's equation [9] to determine the thickness of the anode coating. Diethorn's equation could also be used to determine the increase in gas density due to outgassing from the anode. In using Diethorn's equation in this situation care should be taken to make sure the detector is being operated in a region of gas gain where Diethorn's equation applies (see chapter 9).

Two more experiments were performed with much smaller percentages of DMB. In the first of these experiments the detector ( always detector 1 ) was filled with xenon plus 0.23% DMB to a pressure of 200.4 torr at 0°C. This gas mixture gave the maximum gas gains for a particular range of operating voltages of any xenon plus DMB mixture at this particular gas density ( see chapter 10 ). Throughout the experiment the operating voltage for the detector was 600 volts giving an initial gas gain of \( \sim 562 \). The radiation source was \( ^{55}\text{Fe} \) and the count rate for the full energy peak was 9567 counts per second. The preamplifier and pulse height analyser were connected when pulse height distributions were required and were left connected for long periods of time but often the detector anode was connected directly to the high voltage and the cathode was connected directly to ground. The detector was irradiated for 232 hours and 11 minutes, approximately 10 days and during this time the peak in the pulse height distribution moved from channel 528 to channel 350. The resolution of the detector at 5.9 keV changed from \( \sim 26\% \) to \( \sim 30\% \) and the pulse height distribution seemed to retain its gaussian shape. There was no sign of a double peak. The channel number as a function of time is shown below in Figure 12.2.4.
Figure 12.2.4
The channel number as a function of time for the full energy peak. The gas mixture was xenon plus 0.23% DMB at a pressure of 200.4 torr at 0°C, the radiation source was $^{55}$Fe and the count rate was \(~9,600\) counts per second. The operating voltage for the detector was 600 volts.

The points seem to show a daily variation superimposed upon a general downward trend. In the mornings there was a rapid drop in the channel number for the full energy peak and in the afternoons there was virtually no change at all. The daily variation was probably due to drift in the electronics. To test out this idea a test pulse of fixed amplitude was applied at various times during the day and a pulse height distribution of the test pulses obtained. The test pulses gave a pulse height distribution of \(~18\%\) FWHM and showed a variation of seven channels between 9.25 am and 2.15 pm. Between 9.15 am and 2.20 pm the full energy peak of the pulse height spectrum due to the radiation source changed from channel 367 to channel 351, consequently when electronic drift is allowed.
for, the real change would be a change of 9 channels rather than 16 channels. The general downward trend apparent in the data points should be a reasonably accurate indication of the rate at which the detector gain drops with time as a result of constant irradiation. After 232 hours and 11 minutes of irradiation the anode was "flashed" without removing the gas filling. A voltage of 33 V r.m.s. was applied across the anode causing a current of ~ 0.7 A r.m.s. to pass through the anode and a red glow was observed. The effect of flashing the anode was to reduce the gas gain even further. The full energy peak moved from channel 350 to channel 286 and the energy resolution changed from ~ 30% to ~ 33% FWHM. The anode was flashed a second time without removing the gas filling. This time 20 V r.m.s. was applied and a current of ~ 0.7 A r.m.s. was measured flowing through the anode. A red glow was once again observed with what appeared to be red flashes. After the second flashing the full energy peak moved to channel 248 and the resolution changed to ~ 36% FWHM at 5.9 keV. At this stage the experiment was concluded and the anode was replaced.

For the next experiment the detector (with a new 70 µm diameter anode) was filled with a mixture of xenon plus 4.19% DMB to a pressure of 201.5 torr at 0°C. The detector was operated at 800 volts for 239 hours and 14 minutes. The operating voltage of 800 volts gave a gas gain similar to that obtained at 600 volts with the previous mixture. The radiation source was 55Fe and the count rate was 9577 counts per second. This means that the initial gas gain, duration of experiment and count rates for this mixture and the previous mixture are roughly the same allowing a comparison to be drawn. Figure 12.2.5 shows the channel number of the full energy peak as a function of time.
Figure 12.2.5
The channel number of the full energy peak as a function of time. The gas mixture was xenon plus 4.19% DMB at a pressure of 201.5 torr at 0°C, the radiation source was $^{55}$Fe, the count rate was $\sim 9,600$ counts per second and the operating voltage was 800 volts.

With xenon plus 4.19% DMB the decrease in channel number as a function of time takes on an almost exponential appearance (see Figure 12.2.5 above). Over the $\sim 10$ day period the energy resolution changed from $\sim 23.6\%$ FWHM to $\sim 28.1\%$ FWHM and the full energy peak moved from channel 512 to channel 445. This represents a change in gain of only 13% compared with the 0.23% DMB mixture which underwent a change in gain of 33.7%. Once again this mixture did not develop double full energy peaks.

The results from the experiments given in this section indicate that mixtures of xenon plus 27.14% DMB at pressures of $\sim 200$ torr at 0°C will give rise to
double full energy peaks whereas mixtures of xenon plus 0.23% DMB and mixtures of xenon plus 4.19% DMB at similar densities do not. This indicates that with the mixture with the largest concentration of DMB the electron avalanches are confined to a small region of the anode despite the gas gains of ~2,500 whereas in the mixtures consisting of smaller concentrations of DMB the electron avalanches probably totally surround the anode even though the gas gain is approximately 500-600. This would support the view presented in chapter 11. In this chapter it was suggested that the large gas gains observed in xenon plus small concentrations of DMB was due to the formation of vibrationally excited xenon molecules in three body collisions which radiate UV photons of energy ~8 eV. These UV photons ionize the DMB with great efficiency. If this were an accurate description of what occurs in these gas mixtures then the electron avalanches might totally surround the anode.

The above results are considered to be only preliminary results in this area of investigation.

12.3 Simple theory of detector ageing

The simple theory of detector ageing presented here assumes that the gas filling contains a component or components with covalent bonds. The ageing of such a detector may be the result of the formation of free radicals in the gas filling [10] as a result of the primary ionization or in the electron avalanche. The energy required to break covalent bonds can be considerably less than the ionization potential of the particular molecule, for example the energy required to break the C-C bond is only 3.6 eV, the C-H bond requires 4.3 eV and a C=C bond requires 6.4 eV [10]. A DMB molecule possesses all these bonds but has an ionization potential of 8.30 eV [11]. As little as 3.60 eV is required to break up the molecule. The fragments formed will be free radicals which are highly reactive. According to Bell et. al., as noted by Va’vra [10], under plasma chemistry conditions, which seem to be different in many respects to the conditions thought to exist in electron avalanches, the concentrations of free radicals can be 5 or 6 orders of magnitude greater than the concentration of ions. The plasma chemistry conditions referred to involve similar energies to those that seem to occur in electron avalanches (~10 eV) but much larger effective volumes, smaller typical electron densities, and much lower gas densities. The free radicals are usually deformed and as a consequence have large electric dipole moments. As a result of the strength of the electric field the free radicals will align themselves with the field. In proportional counters with the central wire as the anode the field will have a strong gradient near the anode and as a consequence the free radicals will drift towards the anode. At the anode the free radicals will be held by electrostatic attraction and because these molecules are highly reactive requiring an activation energy of zero to take part in a chemical
reaction they polymerize on the surface of the anode. When a molecule, which is not a free radical itself, reacts with a free radical the product can be another free radical so chain propagation results.

The above description probably describes the ageing effects observed in the experiments presented in the preceding section. If some sort of "free radical trap" or "scavenger" molecule can be added to the gas the polymerization might be halted.

Sipila et. al. [12] has been able to extend the lifespan of detectors filled with P-10 by adding a small amount of hydrogen gas. In the electron avalanches with P-10 the CH₄ molecule can dissociate into various products. The main dissociation product might be CH₂ [13], and CH [14] has also been identified in an optical spectrum of avalanches. Sipila et. al. [12] gives the following possible sequence of events for the polymerization process.

\[
\text{CH}_2 + \text{CH}_4 \rightarrow \text{C}_2\text{H}_6 \\
\text{C}_2\text{H}_6 + \text{CH}_2 \rightarrow \text{C}_3\text{H}_8
\]

They suggest that the above process continues until the deposit becomes solid and consequently cannot diffuse away from the surface of the anode. Sipila et. al. [12] point out that the above process is oversimplified since other radicals and their excited states are also present. They assumed that adding hydrogen to the gas would slow down the polymerization process. The amount of hydrogen added was small, from 0.1 to 0.5%. The effect was to extend the lifespan of detectors filled with P-10 by a factor of 20.

Of course it would be even better if the process of ageing could be halted altogether.

### 12.4 Immortal mixtures

Dwurazny et. al. [15] have reported gas mixtures which show no ageing below \( \sim 5 \times 10^{18} \) electrons per cm of anode. Unfortunately Sipila et. al. [12] do not express their results in electrons per cm of anode so it is difficult to compare these results with theirs. Theoretically Dwurazny et. al.'s mixtures should be immortal mixtures. They found that Ar + 8% N₂ and Ar + 10%Kr + 3.5%H₂ showed no deterioration after accumulating \( 5 \times 10^{18} \) electrons/cm of anode whilst deterioration was observed in Ar + 4%iso-C₅H₁₂ after collecting \( \sim 2 \times 10^{17} \) e/cm.

Ostrowski et. al. [16] give Xe + Kr + H₂ as a long lived mixture. According to these authors, in the above mixture complexes of the form XeKrH₂⁺ are the charge carriers for the positive charges. These complexes neutralize themselves
at the cathode and dissociate into neutral components, i.e. Xe, Kr and H₂. These complexes form as a result of two or more three body collisions, and have stable lifetimes of ~200 µseconds.

12.5 Conclusion

If proportional counters are to be used on long space missions it seems desirable for them to have long lifespans. Very little is known about the ageing of detectors at the moment but Sipila et. al.'s [12] success with adding H₂ to P-10 seems to suggest that something positive can be done to lengthen the lifespan of cylindrical proportional counters. Ageing studies with detectors with uniform fields in the region of the avalanche remain to be done.

References